HALL

FUNDAMENTALS OF CHEMICAL ENGINEERING THERMODYNAMICS

WITH APPLICATIONS TO CHEMICAL PROCESSES

THEMIS MATSOUKAS



FREE SAMPLE CHAPTER









SHARE WITH OTHERS

Fundamentals of Chemical Engineering Thermodynamics

Prentice Hall International Series in the Physical and Chemical Engineering Sciences



Visit informit.com/ph/physandchem for a complete list of available publications.

The Prentice Hall International Series in the Physical and Chemical Engineering Sciences had its auspicious beginning in 1956 under the direction of Neal R. Amundsen. The series comprises the most widely adopted college textbooks and supplements for chemical engineering education. Books in this series are written by the foremost educators and researchers in the field of chemical engineering.



Make sure to connect with us! informit.com/socialconnect







PFAR

Fundamentals of Chemical Engineering Thermodynamics

Themis Matsoukas



Upper Saddle River, NJ • Boston • Indianapolis • San Francisco New York • Toronto • Montreal • London • Munich • Paris • Madrid Capetown • Sydney • Tokyo • Singapore • Mexico City Many of the designations used by manufacturers and sellers to distinguish their products are claimed as trademarks. Where those designations appear in this book, and the publisher was aware of a trademark claim, the designations have been printed with initial capital letters or in all capitals.

The author and publisher have taken care in the preparation of this book, but make no expressed or implied warranty of any kind and assume no responsibility for errors or omissions. No liability is assumed for incidental or consequential damages in connection with or arising out of the use of the information or programs contained herein.

The publisher offers excellent discounts on this book when ordered in quantity for bulk purchases or special sales, which may include electronic versions and/or custom covers and content particular to your business, training goals, marketing focus, and branding interests. For more information, please contact:

U.S. Corporate and Government Sales (800) 382-3419 corpsales@pearsontechgroup.com

For sales outside the United States please contact:

International Sales international@pearson.com

Visit us on the Web: informit.com/ph

Library of Congress Cataloging-in-Publication Data

Matsoukas, Themis. Fundamentals of chemical engineering thermodynamics : with applications to chemical processes / Themis Matsoukas. p. cm. Includes bibliographical references and index. ISBN 0-13-269306-2 (hardcover : alk. paper)

1. Thermodynamics—Textbooks. 2. Chemical engineering—Textbooks. I. Title.

QD504.M315 2013 660—dc23

2012025140

Copyright © 2013 Pearson Education, Inc.

All rights reserved. Printed in the United States of America. This publication is protected by copyright, and permission must be obtained from the publisher prior to any prohibited reproduction, storage in a retrieval system, or transmission in any form or by any means, electronic, mechanical, photocopying, recording, or likewise. To obtain permission to use material from this work, please submit a written request to Pearson Education, Inc., Permissions Department, One Lake Street, Upper Saddle River, New Jersey 07458, or you may fax your request to (201) 236-3290.

ISBN-13: 978-0-13-269306-6 ISBN-10: 0-13-269306-2

Text printed in the United States on recycled paper at Edwards Brothers Malloy in Ann Arbor, Michigan. First printing, September 2012 Executive Editor Bernard Goodwin

Managing Editor John Fuller

Production Editor Elizabeth Ryan

Packager Michelle Gardner

Copy Editor Alyson Platt

Indexer Constance Angelo

Proofreader Gina Delaney

Cover Designer Alan Clements

Compositor Laserwords To my mother, Vana, $${\rm TM}$$

Prefa	ice	xiii
Ackn	owledgments	xvii
Abou	t the Author	xix
Nom	enclature	ххі
Part	I Pure Fluids	1
Chap	ter 1 Scope and Language of Thermodynamics	3
1.1	Molecular Basis of Thermodynamics	5
1.2	Statistical versus Classical Thermodynamics	11
1.3	Definitions	13
	Units	22
1.5	Summary	26
1.6	Problems	26
Chap	ter 2 Phase Diagrams of Pure Fluids	29
2.1	The PVT Behavior of Pure Fluid	29
2.2	Tabulation of Properties	40
2.3	Compressibility Factor and the ZP Graph	43
2.4	Corresponding States	45
2.5	Virial Equation	53
2.6	Cubic Equations of State	57
2.7	<i>PVT</i> Behavior of Cubic Equations of State	61
2.8	Working with Cubic Equations	64
2.9	Other Equations of State	67
2.10	Thermal Expansion and Isothermal Compression	71
2.11	Empirical Equations for Density	72
2.12	5	77
2.13	Problems	78

Chapt	er 3 Energy and the First Law	87		
3.1				
3.2	3.2 Shaft Work and <i>PV</i> Work			
3.3				
3.4				
3.5	Elementary Paths	101		
3.6	Sensible Heat—Heat Capacities	109		
3.7	Heat of Vaporization	119		
3.8	Ideal-Gas State	124		
3.9	Energy Balances and Irreversible Processes	133		
3.10	Summary	139		
3.11	Problems	140		
Chapt	er 4 Entropy and the Second Law	149		
4.1	The Second Law in a Closed System	150		
4.2	Calculation of Entropy	153		
4.3	Energy Balances Using Entropy	163		
4.4	Entropy Generation	167		
4.5	Carnot Cycle	168		
4.6	Alternative Statements of the Second Law	177		
4.7	Ideal and Lost Work	183		
4.8 Ambient Surroundings as a Default Bath—Exergy				
4.9	Equilibrium and Stability	191		
4.10	Molecular View of Entropy	195		
4.11	Summary	199		
4.12	Problems	201		
Chapt	er 5 Calculation of Properties	205		
5.1	Calculus of Thermodynamics	205		
	Integration of Differentials	213		
5.3	Fundamental Relationships	214		
5.4	Equations for Enthalpy and Entropy	217		
	Ideal-Gas State	219		
5.6	Incompressible Phases	220		
5.7	Residual Properties	222		
5.8	5.8 Pressure-Explicit Relations 2			
5.9	Application to Cubic Equations	230		
5.10	5.10 Generalized Correlations 23			
5.11	Reference States	236		

5.12	Thermodynamic Charts	242	
5.13	Summary	245	
5.14	Problems	246	
Chap	ter 6 Balances in Open Systems	251	
6.1	Flow Streams	252	
6.2	Mass Balance	253	
6.3	Energy Balance in Open System	255	
6.4			
6.5	5 Ideal and Lost Work		
6.6	Thermodynamics of Steady-State Processes	272	
6.7	Power Generation	295	
6.8	Refrigeration	301	
6.9	Liquefaction	309	
6.10	Unsteady-State Balances	315	
6.11	Summary	323	
6.12	Problems	324	
Chap	ter 7 VLE of Pure Fluid	337	
7.1	Two-Phase Systems	337	
7.2	Vapor-Liquid Equilibrium	340	
7.3	Fugacity	343	
7.4	Calculation of Fugacity	345	
7.5	Saturation Pressure from Equations of State	353	
7.6	Phase Diagrams from Equations of State	356	
7.7	Summary	358	
7.8	Problems	360	
Part	t II Mixtures	367	
r ar i		307	
Chap		369	
8.1	The <i>Txy</i> Graph	370	
8.2	The <i>Pxy</i> Graph	373	
8.3	Azeotropes 38		
8.4	The xy Graph 33		
8.5	VLE at Elevated Pressures and Temperatures		
8.6	Partially Miscible Liquids 3		
8.7	Ternary Systems 3		

8.8	Summary	393
8.9	Problems	394
Chapt	ter 9 Properties of Mixtures	401
9.1	Composition	402
9.2	Mathematical Treatment of Mixtures	404
9.3	Properties of Mixing	409
9.4	Mixing and Separation	411
9.5	Mixtures in the Ideal-Gas State	413
9.6	Equations of State for Mixtures	419
9.7	Mixture Properties from Equations of State	421
9.8	Summary	428
9.9	Problems	428
Chapt	ter 10 Theory of Vapor-Liquid Equilibrium	435
10.1	Gibbs Free Energy of Mixture	435
10.2	Chemical Potential	439
10.3	Fugacity in a Mixture	443
10.4	Fugacity from Equations of State	446
10.5	VLE of Mixture Using Equations of State	448
10.6	Summary	453
10.7	Problems	454
Chap	ter 11 Ideal Solution	461
11.1	Ideality in Solution	461
11.2	Fugacity in Ideal Solution	464
11.3	VLE in Ideal Solution–Raoult's Law	466
11.4	Energy Balances	475
11.5	Noncondensable Gases	480
11.6	Summary	484
11.7	Problems	484
Chap	ter 12 Nonideal Solutions	489
12.1	Excess Properties	489
12.2	Heat Effects of Mixing	496
12.3	Activity Coefficient	504
12.4	Activity Coefficient and Phase Equilibrium	507
12.5	Data Reduction: Fitting Experimental Activity Coefficients	512
12.6	Models for the Activity Coefficient	515
12.7	Summary	531
12.8	Problems	533

Chapter 13 Miscibility, Solubility, and Other Phase Equilibria	545	
13.1 Equilibrium between Partially Miscible Liquids		
13.2 Gibbs Free Energy and Phase Splitting		
13.3 Liquid Miscibility and Temperature	556	
13.4 Completely Immiscible Liquids	558	
13.5 Solubility of Gases in Liquids	563	
13.6 Solubility of Solids in Liquids	575	
13.7 Osmotic Equilibrium	580	
13.8 Summary	586	
13.9 Problems	586	
Chapter 14 Reactions	593	
14.1 Stoichiometry	593	
14.2 Standard Enthalpy of Reaction	596	
14.3 Energy Balances in Reacting Systems		
14.4 Activity	606	
14.5 Equilibrium Constant		
14.6 Composition at Equilibrium		
14.7 Reaction and Phase Equilibrium		
14.8 Reaction Equilibrium Involving Solids		
14.9 Multiple Reactions		
14.10 Summary		
14.11 Problems	637	
Bibliography	647	
Appendix A Critical Properties of Selected Compounds	649	
Appendix B Ideal-Gas Heat Capacities	653	
Appendix C Standard Enthalpy and Gibbs Free Energy of Reaction	655	
Appendix D UNIFAC Tables	659	
Appendix E Steam Tables	663	
Index	677	

Preface

My goal with this book is to provide the undergraduate student in chemical engineering with the solid background to perform thermodynamic calculations with confidence, and the course instructor with a resource to help students achieve this goal. The intended audience is sophomore/junior students in chemical engineering. The book is divided into two parts. Part I covers the laws of thermodynamics, with applications to pure fluids; Part II extends thermodynamics to mixtures, with emphasis on phase and chemical equilibrium. The selection of topics was guided by the realities of the undergraduate curriculum, which gives us about 15 weeks per semester to develop the material and meet the learning objectives. Given that thermodynamics requires some minimum "sink-in" time, the deliberate choice was made to prioritize topics and cover them at a comfortable pace. Each part consists of seven chapters, corresponding to an average of about two weeks (six lectures) per chapter. Under such restrictions certain topics had to be left out and for others their coverage had to be limited. Highest priority is given to material that feeds directly to other key courses of the curriculum: separations, reactions, and capstone design. A deliberate effort was made to stay away from specialty topics such as electrochemical or biochemical systems on the premise that these are more appropriately dealt with (and at a depth that a book such as this could do no justice) in physical chemistry, biochemistry, and other dedicated courses. Students are made aware of the amazing generality of thermodynamics and are directed to other fields for such details as needed. A theme that permeates the book is the molecular basis of thermodynamics. Discussions of molecular phenomena remain at a qualitative level (except for very brief excursions to statistical concepts in the chapter on entropy), consistent with the background of the typical sophomore/junior. But the molecular picture is consistently brought up to reinforce the idea that the quantities we measure in the lab and the equations that describe them are manifestations of microscopic effects at the molecular level.

The two parts of the book essentially mirror the material of a two-course sequence in thermodynamics that is typically required in chemical engineering. The focus of Part I is on pure fluids exclusively. The PVT behavior is introduced early on (Chapter 2) so that when it comes to the first and second law (Chapters 3 and 4), students have the tools to perform basic calculations of enthalpy and entropy using steam tables (a surrogate for tabulated properties in general) and equations of state. Chapter 5 discusses fundamental relationships and the calculation of properties from equations of state. It is mathematically the densest chapter of Part I.

Chapter 6 goes into applications of thermodynamics to chemical processes. The range of applications is limited to systems involving pure fluids, namely power plants and refrigeration/liquefaction systems. This is the part of the course that most directly relates to processes discussed in capstone design and justifies the "Chemical Engineering" in the title of the book. It is one of the longer chapters, with several examples and end-of-chapter problems. The last chapter in this part covers phase equilibrium for a single fluid and serves as the connector between the two parts, as fugacity is the main actor in Part II.

The second part begins with a survey of phase diagrams of binary and simple ternary systems. It introduces the variety of phase behaviors of mixtures and establishes the notion that each phase at equilibrium has its own composition, and introduces the lever rule as a basic material balance tool. Many programs probably cover some of that material in the Materials and Energy Balances course but the topics are central to subsequent discussions so that a separate chapter is justified. Chapter 9 extends the fundamental relationships, which in Part I were applied to pure fluids, to mixtures. This chapter also introduces the equation of state for mixtures and the calculation of mixture properties from the equation of state. Chapter 10 is a short chapter that establishes the phase equilibrium criterion for mixtures and applies the equation of state to calculate the phase diagram of a binary mixture. Chapters 11 and 12 deal with ideal and nonideal solutions, respectively. Chapter 13 goes over several topics of phase equilibrium that are too small to be in separate chapters. These include partial miscibility, solubility of gases and solids, and osmotic processes. The last chapter in this part, 14, covers reaction equilibrium. The focus of the chapter is to establish the fundamental relationships, which are then applied to single and multiphase reactions. Standard states are discussed in quite some detail, since this is a topic that seems to confuse students.

Overall, a great effort has been made to balance theory with examples and applications. Examples cover a wide range, from direct application of formulas and methodologies, to larger processes that require synthesis of several smaller problems. It has been my experience that students are more willing to accept what they perceive as abstract theory if they can see how this theory is tied to practical industrial situations. Realistic problems are rarely of the paper-and-pencil type, and this brings up the need for mathematical/computational tools. The choices today are many, from sophisticated hand calculators to spreadsheets and numerical packages. The textbook takes an agnostic approach when it comes to the type of software and leaves it up to the instructor to make that choice. Typically, the problems that require numerical tools are those involving calculations with equations of state. Some problems lend themselves to the use of process simulators but, by deliberate decision, there is no specific mention of these simulators in the book. As with the other computational tools, the choice is left to the instructor. In my experience, the

Preface

best approach with problems that require a significant number of computations is to assign them as projects. Picking problems with industrial flavor not only motivates students in engineering, it also offers convincing justification for the practical need for theory and numerical methodologies.

—Themis Matsoukas University Park May 2012

Acknowledgments

This book is the product of some 20 years of teaching thermodynamics at Penn State, but it would not have happened without the help, direct or indirect, of several individuals, colleagues, students, and friends. I must start by thanking Andrew Zydney, my colleague and department head, who encouraged me to spend my 2010–2011 sabbatical finishing this textbook. Without Andrew's nudging, the book would have remained in the perpetual state of a draft-in-progress. I want to thank my colleagues, Darrell Velegol, Scott Milner, Seong Kim, Rob Rioux, and Enrique Gomez, who trusted drafts of the book, in various stages of completion, for use in their classes. Among those who reviewed the near-final draft, I want to thank Michael M. Domach and Tracy J. Benson, who offered comments that were especially insightful and encouraging. The number of students, whose feedback over the years shaped this book, is too large to list. But special thanks must go to my Fall 2011 class of CH E 220H, the honors section of Thermo I, on whom fell the unenviable task of debugging the first finished version of this book. They did this admirably. Of all the students in that class special mention goes to Steph Nitopi, Twafik Miral, Brian Brady, and Ashlee Smith, whose attention to detail was nothing but extraordinary. Bernard Goodwin and Michelle Housley of Pearson Education guided me through this book project—my first one—with a light hand and flexible deadlines. I want to thank Elizabeth Ryan, John Fuller, and Michelle Gardner, who, as members of the production team, brought my vision of this book to life. My wife Kristen, and daughter Melina, helped in many ways, big and small, in carrying this project out. And lastly, I feel grateful to LuLu, our little dog, who sat approvingly on my armchair next to me through countless hours of typing.

About the Author



Themis Matsoukas is a professor of chemical engineering at Pennsylvania State University. He received a diploma in chemical engineering from the National Metsovion Polytechnic School in Athens Greece, and a Ph.D. from the University of Michigan in Ann Arbor. He has taught graduate and undergraduate thermodynamics, materials, and energy balances, and various electives in particle and aerosol technology. Since 1991, he has taught thermodynamics to more than 1000 students at Penn State. He has been recognized with several awards for excellence in teaching and advising.

Nomenclature

In general, properties are assumed to be molar unless indicated differently. A corresponding extensive property is indicated by the superscript ^{tot}, for example, $H^{\text{tot}} = nH$. In dealing with mixtures, a variable without subscripts or superscripts (e.g., H) is the molar property of the mixture; a property with a subscript (e.g., H_i) is the corresponding property of the pure component; a property with an overbar (e.g., \overline{H}_i) is the partial molar property of the component in the mixture.

List of Symbols

A	Helmholtz free energy, $A = U - TS$
a_i	activity of component i
F	generic thermodynamic property
f	fugacity of component
G	Gibbs free energy, $G = H - TS$
\overline{G}_i	partial molar Gibbs free energy
G^E	excess Gibbs free energy
\overline{G}_i^E	excess partial molar Gibbs free energy
G^R	residual Gibbs free energy
\overline{G}_i^R	residual partial molar Gibbs free energy
G°	standard Gibbs energy of formation
Н	enthalpy, $H = U + PV$
\overline{H}_i	partial molar enthalpy
H^E	excess enthalpy
\overline{H}_{i}^{E}	excess partial molar enthalpy
H^R	residual enthalpy
\overline{H}_{i}^{R}	residual partial molar enthalpy
H°	standard enthalpy of formation
$\Delta H_{\rm vap}$	enthalpy or heat of vaporization
$\Delta H_{\rm mix}$	enthalpy or heat of mixing
K	equilibrium constant

k_B	Boltzmann constant
k_{ij}	interaction parameter in equation of state
k_i^H	Henry's law constant for component i
$k_i^{H'}$	Henry's law constant for component i based on molality
k_{ij}	interaction parameter in equation of state
L	liquid fraction of a vapor-liquid mixture
m	mass
n	number of moles
N	number of components
$P^{\rm sat}$	saturation pressure
Q	heat
R	ideal-gas constant, $R = 8.314 \text{ J/mol K}$
S	entropy
\bar{S}_i	partial molar entropy
S^E	excess entropy
${ar{S}}_i^E$	excess partial molar entropy
S^R	residual entropy
\bar{S}_{i}^{R}	residual partial molar entropy
S°	standard entropy of formation
ΔS_{vap}	entropy of vaporization
$\Delta S_{ m mix}$	entropy of mixing
$\Delta S_{ m mix}^{ m id}$	ideal entropy of mixing, $\Delta S_{\text{mix}}^{\text{id}} = -R \sum x_i \ln x_i$
U	internal energy
V	volume; also used to denote the vapor fraction of a vapor-liquid mixture
W	work
w_i	mass fraction
x_i	generic mole fraction or mol fraction in liquid (two-phase system)
y_i	mole fraction in gas (two-phase system)
z_i	overall mole fraction in two-phase system

Greek symbols

β	volumetric coefficient of thermal expansion
γ	activity coefficient

Nomenclature

κ	coefficient of isothermal compressibility
μ	chemical potential
ν	stoichiometric coefficient
ξ	extent of reaction
π	number of phases (in Gibbs's phase rule)
ρ	density coefficient
ϕ	fugacity
ω	acentric factor

Subscripts

i	component or stream
L	liquid
V	vapor
gen	generation
sur	surroundings
univ	universe

Superscripts

tot	total (extensive) property, for example, $H^{\text{tot}} = nH$
R	residual
ig	ideal-gas state
igm	ideal-gas mixture
id	ideal solution
E	excess
sat	saturation
vap	vaporization
0	standard state

Part I Pure Fluids

Chapter 1

Scope and Language of Thermodynamics

Chemical processes involve streams undergoing various transformations. One example is shown in Figure 1-1: raw materials are fed into a heated reactor, where they react to form products. The effluent stream, in this case a liquid, contains the products of the reaction, any unreacted raw materials, and possibly other by-products. This stream is pumped out of the reactor into a heat exchanger, where it partially boils. The vapor/liquid mixture is fed into a tank, which collects the vapor at the top, and liquid at the bottom. The streams that exit this tank are finally cooled down and sent to the next stage of the process. Actual processes are generally more complex and may involve many streams and several interconnected units. Nonetheless, the example in Figure 1-1 contains all the basic ingredients likely to be found in any chemical plant: heating, cooling, pumping, reactions, phase transformations.

It is the job of the chemical engineer to compute the material and energy balances around such process: This includes the flow rates and compositions of all streams, the power requirements of pumps, compressors and turbines, and the heat loads in the heat exchangers. The chemical engineer must also determine the conditions of pressure and temperature that are required to produce the desired effect, whether this is a chemical reaction or a phase transformation. All of this requires the knowledge of various physical properties of a mixture: density, heat capacity, boiling temperature, heat of vaporization, and the like. More specifically, these properties must be known as a function of temperature, pressure, and composition, all of which vary from stream to stream. Energy balances and property estimation may appear to be separate problems, but they are not: both calculations require the application of the same fundamental principles of thermodynamics.

The name *thermodynamics* derives from the Greek *thermotis* (heat) and *dynamiki* (potential, power). Its historical roots are found in the quest to develop heat engines, devices that use heat to produce mechanical work. This quest, which was instrumental in powering the industrial revolution, gave birth to thermodynamics as a discipline that studies the relationship between heat, work, and energy. The elucidation of this relationship is one of the early triumphs of thermodynamics and a reason why, even today, thermodynamics is often described as the study of energy



Figure 1-1: Typical chemical process.

conversions involving heat. Modern thermodynamics is a much broader discipline whose focus is the equilibrium state of systems composed of very large numbers of molecules. Temperature, pressure, heat, and mechanical work, as manifested through the expansion and compression of matter, are understood to arise from interactions at the molecular level. Heat and mechanical work retain their importance but the scope of the modern discipline is far wider than its early developers would have imagined, and encompasses many different systems containing huge numbers of "particles," whether these are molecules, electron spins, stars, or bytes of digital information. The term *chemical thermodynamics* refers to applications to molecular systems.



Figure 1-2: J. W. Gibbs.

Among the many scientists who contributed to the development of modern thermodynamics, J. Willard Gibbs stands out as one whose work revolutionized the

1.1 Molecular Basis of Thermodynamics

discipline by providing the tools to connect the macroscopic properties of thermodynamics to the microscopic properties of molecules. His name is now associated with the *Gibbs free energy*, a thermodynamic property of fundamental importance in phase and chemical equilibrium.

Chemical engineering thermodynamics is the subset that applies thermodynamics to processes of interest to chemical engineers. One important task is the calculation of energy requirements of a process and, more broadly, the analysis of energy utilization and efficiency in chemical processing. This general problem is discussed in the first part of the book, Chapters 2 through 7. Another important application of chemical engineering thermodynamics is in the design of separation units. The vapor-liquid separator in Figure 1-1 does more than just separate the liquid portion of the stream from the vapor. When a multicomponent liquid boils, the more volatile ("lighter") components collect preferentially in the vapor and the less volatile ("heavier") ones remain mostly in the liquid. This leads to partial separation of the initial mixture. By staging multiple such units together, one can accomplish separations of components with as high purity as desired. The determination of the equilibrium composition of two phases in contact with each other is an important goal of chemical engineering thermodynamics. This problem is treated in the second part of the book and the first part is devoted to the behavior of single-component fluids. Overall then, the chemical engineer uses thermodynamics to

- 1. Perform energy and material balances in unit operations with chemical reactions, separations, and fluid transformations (heating/cooling, compression/ expansion),
- 2. Determine the various physical properties that are required for the calculation of these balances,
- 3. Determine the conditions of equilibrium (pressure, temperature, composition) in phase transformations and chemical reactions.

These tasks are important for the design of chemical processes and for their proper control and troubleshooting. The overall learning objective of this book is to provide the undergraduate student in chemical engineering with a solid background to perform these calculations with confidence.

1.1 Molecular Basis of Thermodynamics

All macroscopic behavior of matter is the result of phenomena that take place at the microscopic level and arise from force interactions among molecules. Molecules exert a variety of forces: direct electrostatic forces between ions or permanent dipoles;

induction forces between a permanent dipole and an induced dipole; forces of attraction between nonpolar molecules, known as van der Waals (or dispersion) forces; other specific chemical forces such as hydrogen bonding. The type of interaction (attraction or repulsion) and the strength of the force that develops between two molecules depends on the distance between them. At far distances the force is zero. When the distance is of the order of several Å, the force is generally attractive. At shorter distances, short enough for the electron clouds of the individual atoms to begin to overlap, the interaction becomes very strongly repulsive. It is this strong repulsion that prevents two atoms from occupying the same point in space and makes them appear as if they possess a solid core. It is also the reason that the density of solids and liquids is very nearly independent of pressure: molecules are so close to each other that adding pressure by any normal amounts (say 10s of atmospheres) is insufficient to overcome repulsion and cause atoms to pack much closer.

Intermolecular Potential The force between two molecules is a function of the distance between them. This force is quantified by intermolecular potential energy, $\Phi(r)$, or simply *intermolecular potential*, which is defined as the work required to bring two molecules from infinite distance to distance r. Figure 1-3 shows the approximate intermolecular potential for CO₂. Carbon dioxide is a linear molecule and its potential depends not only on the distance between the molecules but also on their relative orientation. This angular dependence has been averaged out for simplicity. To interpret Figure 1-3, we recall from mechanics that force is equal to the negative derivative of the potential with respect to distance:

$$F = -\frac{d\Phi(r)}{dr}.$$
(1.1)

That is, the magnitude of the force is equal to the slope of the potential with a negative sign that indicates that the force vector points in the direction in which the potential decreases. To visualize the force, we place one molecule at the origin and a test molecule at distance r. The magnitude of the force on the test molecule is equal to the derivative of the potential at that point (the force on the first molecule is equal in magnitude and opposite in direction). If the direction of force is towards the origin, the force is attractive, otherwise it is repulsive. The potential in Figure 1-3 has a minimum at separation distance $r_* = 4.47$ Å. In the region $r > r_*$ the slope is negative and the force is attractive. The attraction is weaker at longer distances and for r larger than about 9 Å the potential is practically flat and the force is zero. In the region $r < r_*$ the potential is repulsive and its steep slope indicates a very strong force that arises from the repulsive interaction of the electrons surrounding the molecules. Since the molecules cannot be pushed much closer than about $r \approx r_*$,



Figure 1-3: Approximate interaction potential between two CO₂ molecules as a function of their separation distance. The potential is given in kelvin; to convert to joule multiply by the Boltzmann constant, $k_B = 1.38 \times 10^{-23}$ J/K. The arrows show the direction of the force on the test molecule in the regions to the left and to the right of r_* .

we may regard the distance r_* to be the effective diameter of the molecule.¹ Of course, even simple molecules like argon are not solid spheres; therefore, the notion of a molecular diameter should not be taken literally.

The details of the potential vary among different molecules but the general features are always the same: Interaction is strongly repulsive at very short distance, weakly attractive at distance of the order of several Å, and zero at much larger distances. These features help to explain many aspects of the macroscopic behavior of matter.

Temperature and Pressure In the classical view of molecular phenomena, molecules are small material objects that move according to Newton's laws of motion, under the action of forces they exert on each other through the potential interaction. Molecules that collide with the container walls are reflected back, and the force of

^{1.} The closest center-to-center distance we can bring two solid spheres is equal to the sum of their radii. For equal spheres, this distance is equal to their diameter.

this collision gives rise to pressure. Molecules also collide among themselves,² and during these collisions they exchange kinetic energy. In a thermally equilibrated system, a molecule has different energies at different times, but the distribution of energies is overall stationary and the same for all molecules. Temperature is a parameter that characterizes the distribution of energies inside a system that is in equilibrium with its surroundings. With increasing temperature, the energy content of matter increases. Temperature, therefore, can be treated as a measure of the amount of energy stored inside matter.

NOTE

Maxwell-Boltzmann Distribution

The distribution of molecular velocities in equilibrium is given by the Maxwell-Boltzmann equation:

$$f(v) = 4\pi v^2 \left(\frac{m}{2\pi k_B T}\right)^{3/2} e^{-mv^2/2k_B T},$$
(1.2)

where *m* is the mass of the molecule, *v* is the magnitude of the velocity, *T* is absolute temperature, and k_B is the Boltzmann constant. The fraction of molecules with velocities between any two values v_1 to v_2 is equal to the area under the curve between the two velocities (the total area under the curve is 1). The velocity v_{max} that corresponds to the maximum of the distribution, the mean velocity \bar{v} , and the mean of the square of the velocity are all given in terms of temperature:

$$v_{\max} = \left(\frac{2k_BT}{m}\right)^{1/2}, \quad \overline{v} = \left(\frac{8k_BT}{\pi m}\right)^{1/2}, \quad \overline{v^2} = \frac{3k_BT}{m}.$$

The Maxwell-Boltzmann distribution is a result of remarkable generality: it is independent of pressure and applies to any material, regardless of composition or phase. Figure 1-4 shows this distribution for water at three temperatures. At the triple point, the solid, liquid, and vapor, all have the same distribution of velocities.

Phase Transitions The minimum of the potential represents a stable equilibrium point. At this distance, the force between two molecules is zero and any small deviations to the left or to the right produce a force that points back to the minimum. A pair of molecules trapped at this distance r_* would form a stable pair if it were not for their kinetic energy, which allows them to move and eventually escape from the minimum. The lifetime of a trapped pair depends on temperature. At high temperature, energies are higher, and the probability that a pair will remain trapped is low. At low temperature a pair can survive long enough to trap additional molecules and form a small cluster of closely packed molecules. This cluster is a nucleus of

^{2.} Molecular collisions do not require solid contact as macroscopic objects do. If two molecules come close enough in distance, the steepness of the potential produces a strong repulsive force that causes their trajectories to deflect.



Figure 1-4: Maxwell-Boltzmann distribution of molecular velocities in water.

the liquid phase and can grow by further collection to form a macroscopic liquid phase. Thus we have a molecular view of vapor-liquid equilibrium. This picture highlights the fact that to observe a vapor-liquid transition, the molecular potential must exhibit a combination of strong repulsion at short distances with weak attraction at longer distances. Without strong repulsion, nothing would prevent matter from collapsing into a single point; without attraction, nothing would hold a liquid together in the presence of a vapor. We can also surmise that molecules that are characterized by a deeper minimum (stronger attraction) in their potential are easier to condense, whereas a shallower minimum requires lower temperature to produce a liquid. For this reason, water, which associates via hydrogen bonding (attraction) is much easier to condense than say, argon, which is fairly inert and interacts only through weak van der Waals attraction.

NOTE

Condensed Phases

The properties of liquids depend on both temperature and pressure, but the effect of pressure is generally weak. Molecules in a liquid (or in a solid) phase are fairly closely packed so that increasing pressure does little to change molecular distances by any appreciable amount. As a result, most properties of liquids are quite insensitive to pressure and can be approximately taken to be functions of temperature only.

Example 1.1: Density of Liquid CO₂

Estimate the density of liquid carbon dioxide based on Figure 1-3.

Solution The mean distance between molecules in the liquid is approximately equal to r_* , the distance where the potential has a minimum. If we imagine molecules to be arranged in a regular cubic lattice at distance r_* from each other, the volume of N_A molecules would be $N_A r_*^3$. The density of this arrangement is

$$\rho = \frac{M_m}{N_{\rm A} r_*^3},$$

where M_m is the molar mass. Using $r_* = 4.47$ Å = 4.47×10^{-9} m, $M_m = 44.01 \times 10^{-3}$ kg/mol,

$$\rho = \frac{44.01 \times 10^{-3} \text{ kg/mol}}{(6.022 \times 10^{23} \text{ mol}^{-1})(4.47 \times 10^{-10} \text{ m})^3} = 818 \text{ kg/m}^3$$

Perry's Handbook (7th ed., Table 2-242) lists the following densities of saturated liquid CO₂ at various temperatures:

$T(\mathbf{K})$	$ ho (kg/m^3)$
216.6	1130.7
270	947.0
300	680.3
304.2	466.2

According to this table, density varies with temperature from 1130.7 kg/m³ at 216.6 K to 466.2 kg/m^3 at 304.2 K. The calculated value corresponds approximately to 285 K.

Comments The calculation based on the intermolecular potential is an estimation. It does not account for the effect of temperature (assumes that the mean distance between molecules is r_* regardless of temperature) and that molecules are arranged in a regular cubic lattice. Nonetheless, the final result is of the correct order of magnitude, a quite impressive result given the minimal information used in the calculation.

Ideal-Gas State Figure 1-3 shows that at distances larger than about 10 Å the potential of carbon dioxide is fairly flat and the molecular force nearly zero. If carbon dioxide is brought to a state such that the mean distance between molecules is more than 10 Å we expect that molecules would hardly register the presence of each other and would largely move independently of each other, except for brief close encounters. This state can be reproduced experimentally by decreasing pressure (increasing volume) while keeping temperature the same. This is called the *ideal-gas state*. It is a *state*—not a gas—and is reached by any gas when pressure is reduced sufficiently. In the ideal-gas state molecules move independently

of each other and without the influence of the intermolecular potential. Certain properties in this state become universal for all gases regardless of the chemical identity of their molecules. The most important example is the ideal-gas law, which describes the pressure-volume-temperature relationship of any gas at low pressures.

1.2 Statistical versus Classical Thermodynamics

Historically, a large part of thermodynamics was developed before the emergence of atomic and molecular theories of matter. This part has come to be known as *clas*sical thermodynamics and makes no reference to molecular concepts. It is based on two basic principles ("laws") and produces a rigorous mathematical formalism that provides exact relationships between properties and forms the basis for numerical calculations. It is a credit to the ingenuity of the early developers of thermodynamics that they were capable of developing a correct theory without the benefit of molecular concepts to provide them with physical insight and guidance. The limitation is that classical thermodynamics cannot explain why a property has the value it does, nor can it provide a convincing physical explanation for the various mathematical relationships. This missing part is provided by statistical thermodynamics. The distinction between classical and statistical thermodynamics is partly artificial, partly pedagogical. Artificial, because thermodynamics makes physical sense only when we consider the molecular phenomena that produce the observed behaviors. From a pedagogical perspective, however, a proper statistical treatment requires more time to develop, which leaves less time to devote to important engineering applications. It is beyond the scope of this book to provide a bottom-up development of thermodynamics from the molecular level to the macroscopic. Instead, our goal is to develop the knowledge, skills, and confidence to perform thermodynamic calculations in chemical engineering settings. We will use molecular concepts throughout the book to shed light to new concepts but the overall development will remain under the general umbrella of classical thermodynamics. Those who wish to pursue the connection between the microscopic and the macroscopic in more detail, a subject that fascinated some of the greatest scientific minds, including Einstein, should plan to take an upper-level course in statistical mechanics from a chemical engineering, physics, or chemistry program.

The Laws of Classical Thermodynamics Thermodynamics is built on a small number of axiomatic statements, propositions that we hold to be true on the basis of our experience with the physical world. Statistical and classical thermodynamics make use of different axiomatic statements; the axioms of statistical thermodynamics have their basis on statistical concepts; those of classical thermodynamics are based on
behavior that we observe macroscopically. There are two fundamental principles in classical thermodynamics, commonly known as the first and second law.³ The first law expresses the principle that matter has the ability to store energy *within*. Within the context of classical thermodynamics, this is an axiomatic statement since its physical explanation is inherently molecular. The second law of thermodynamics expresses the principle that all systems, if left undisturbed, will move towards equilibrium –never away from it. This is taken as an axiomatic principle because we cannot prove it without appealing to other axiomatic statements. Nonetheless, contact with the physical world convinces us that this principle has the force a universal physical law.

Other laws of thermodynamics are often mentioned. The "zeroth" law states that, if two systems are in thermal equilibrium with a third system, they are in equilibrium with each other. The third law makes statements about the thermodynamic state at absolute zero temperature. For the purposes of our development, the first and second law are the only two principles needed in order to construct the entire mathematical theory of thermodynamics. Indeed, these are the only two equations that one must memorize in thermodynamics; all else is a matter of definitions and standard mathematical manipulations.

The "How" and the "Why" in Thermodynamics Engineers must be skilled in the art of *how* to perform the required calculations, but to build confidence in the use of theoretical tools it is also important to have a sense *why* our methods work. The "why" in thermodynamics comes from two sources. One is physical: the molecular picture that gives meaning to "invisible" quantities such as heat, temperature, entropy, equilibrium. The other is mathematical and is expressed through exact relationships that connect the various quantities. The typical development of thermodynamics goes like this:

- (a) Use physical principles to establish fundamental relationships between key properties. These relationships are obtained by applying the first and second law to the problem at hand.
- (b) Use calculus to convert the fundamental relationships from step (a) into useful expressions that can be used to compute the desired quantities.

Physical intuition is needed in order to justify the fundamental relationships in step (a). Once the physical problem is converted into a mathematical one (step [b]),

^{3.} The term *law* comes to us from the early days of science, a time during which scientists began to recognize mathematical order behind what had seemed up until then to be a complicated physical world that defies prediction. Many of the early scientific findings were known as "laws," often associated with the name of the scientist who reported them, for example, Dalton's law, Ohm's law, Mendel's law, etc. This practice is no longer followed. For instance, no one refers to Einstein's famous result, $E = mc^2$, as Einstein's law.

physical intuition is no longer needed and the gear must shift to mastering the "how." At this point, a good handle of calculus becomes indispensable, in fact, a prerequisite for the successful completion of this material. Especially important is familiarity with functions of multiple variables, partial derivatives and path integrations.

1.3 Definitions

System

The system is the part of the physical world that is the object of a thermodynamic calculation. It may be a fixed amount of material inside a tank, a gas compressor with the associated inlet and outlet streams, or an entire chemical plant. Once the system is defined, anything that lies outside the system boundaries belongs to the surroundings. Together system and surroundings constitute the universe. A system can interact with its surroundings by exchanging mass, heat, and work. It is possible to construct the system in such way that some exchanges are allowed while others are not. If the system can exchange mass with the surroundings it called open, otherwise it is called closed. If it can exchange heat with the surroundings it is called diathermal, otherwise it is called adiabatic. A system that is prevented from exchanging either mass, heat, or work is called isolated. The universe is an isolated system.

A simple system is one that has no internal boundaries and thus allows all of its parts to be in contact with each other with respect to the exchange of mass, work, and heat. An example would be a mole of a substance inside a container. A *composite* system consists of simple systems separated by boundaries. An example would be a box divided into two parts by a firm wall. The construction of the wall would determine whether the two parts can exchange mass, heat, and work. For example, a permeable wall would allow mass transfer, a diathermal wall would allow heat transfer, and so on.

Example 1.2: Systems

Classify the systems in Figure 1-5.

Solution In (a) we have a tank that contains a liquid and a vapor. This system is inhomogeneous, because it consists of two phases; closed, because it cannot exchange mass with the surroundings; and simple, because it does not contain any internal walls. Although the liquid can exchange mass with the vapor, the exchange is internal to the system. There is no mention of insulation. We may assume, therefore, that the system is diathermal.

In (b) we have the same setup but the system is now defined to be just the liquid portion of the contents. This system is simple, open, and diathermal. Simple, because there are no internal walls; open, because the liquid can exchange mass with the vapor by evaporation or condensation; and diathermal, because it can exchange heat with the vapor. In this case, the insulation around the tank is not sufficient to render the system adiabatic because of the open interface between the liquid and vapor.

In (c) we have a condenser similar to those found in chemistry labs. Usually, hot vapor flows through the center of the condenser while cold water flows on the outside, causing the vapor to condense. This system is open because it allows mass flow through its boundaries. It is composite because of the wall that separates the two fluids. It is adiabatic because it is insulated from the surroundings. Even though heat is transferred between the inner and outer tube, this transfer is internal to the system (it does not cross the system bounds) and does not make the system diathermal.

Comments In the condenser of part (c), we determined the system to be open and adiabatic. Is it not possible for heat to enter through the flow streams, making the system diathermal? Streams carry energy with them and, as we will learn in Chapter 6, this is in the form of enthalpy. It is possible for heat to cross the boundary of the system inside the flow stream through conduction, due to different temperatures between the fluid stream just outside the system and the fluid just inside it. This heat flows slowly and represents a negligible amount compared to the energy carried by the flow. The main mode heat transfer is through the external surface of the system. If this is insulated, the system may be considered adiabatic.



Figure 1-5: Examples of systems (see Example 1.2). The system is indicated by the dashed line. (a) Closed tank that contains some liquid and some gas. (b) The liquid portion in a closed, thermally insulated tank that also contains some gas. (c) Thermally insulated condenser of a laboratory-scale distillation unit.

Equilibrium

It is an empirical observation that a simple system left undisturbed, in isolation of its surroundings, must eventually reach an ultimate state that does not change with time. Suppose we take a rigid, insulated cylinder, fill half of it with liquid nitrogen at atmospheric pressure and the other half with hot, pressurized nitrogen, and place a wall between the two parts to keep them separate. Then, we rupture the wall between the two parts and allow the system to evolve without any disturbance from the outside. For some time the system will undergo changes as the two parts mix. During this time, pressure and temperature will vary, and so will the amounts of liquid and vapor. Ultimately, however, the system will reach a state in which no more changes are observed. This is the equilibrium state.

Equilibrium in a simple system requires the fulfillment of three separate conditions:

- 1. *Mechanical equilibrium*: demands uniformity of *pressure* throughout the system and ensures that there is no net work exchanged due to pressure differences.
- 2. *Thermal equilibrium*: demands uniformity of *temperature* and ensures no net transfer of heat between any two points of the system.
- 3. *Chemical equilibrium*: demands uniformity of the *chemical potential* and ensures that there is no net mass transfer from one phase to another, or net conversion of one chemical species into another by chemical reaction.

The chemical potential will be defined in Chapter 7.

Although equilibrium appears to be a static state of no change, at the molecular level it is a dynamic process. When a liquid is in equilibrium with a vapor, there is continuous transfer of molecules between the two phases. On an instantaneous basis the number of molecules in each phase fluctuates; overall, however, the molecular rates to and from each phase are equal so that, on average, there is no net transfer of mass from one phase to the other.

Constrained Equilibrium If we place two systems into contact with each other via a wall and isolate them from the rest of their surroundings, the overall system is isolated and composite. At equilibrium, each of the two parts is in mechanical, thermal, and chemical equilibrium at its own pressure and temperature. Whether the two parts establish equilibrium with *each other* will depend on the nature of the wall that separates them. A diathermal wall allows heat transfer and the equilibration of temperature. A movable wall (for example, a piston) allows the equilibration of pressure.

A selectively permeable wall allows the chemical equilibration of the species that are allowed to move between the two parts. If a wall allows certain exchanges but not others, equilibrium is established only with respect to those exchanges that are possible. For example, a fixed conducting wall allows equilibration of temperature but not of pressure. If the wall is fixed, adiabatic, and impermeable, there is no exchange of any kind. In this case, each part establishes its own equilibrium independently of the other.

Extensive and Intensive Properties

In thermodynamics we encounter various properties, for example, density, volume, heat capacity, and others that will be defined later. In general, *property* is any quantity that can be measured in a system at equilibrium. Certain properties depend on the actual amount of matter (size or extent of the system) that is used in the measurement. For example, the volume occupied by a substance, or the kinetic energy of a moving object, are directly proportional to the mass. Such properties will be called *extensive*. Extensive properties are additive: if an amount of a substance is divided into two parts, one of volume V_1 and one of volume V_2 , the total volume is the sum of the parts, $V_1 + V_2$. In general, the total value of an extensive property in a system composed of several parts is the sum of its parts. If a property is independent of the size of the system, it will be called *intensive*. Some examples are pressure, temperature, density. Intensive properties are independent of the amount of matter and are *not* additive.

As a result of the proportionality that exists between extensive properties and amount of material, the ratio of an extensive property to the amount of material forms an intensive property. If the amount is expressed as mass (in kg or lb), this ratio will be called a *specific* property; if the amount is expressed in mole, it will be called a molar property. For example, if the volume of 2 kg of water at 25 °C, 1 bar, is measured to be 2002 cm³, the specific volume is

$$V = \frac{2002 \times 10^{-3} \text{ m}^3}{2 \text{ kg}} = 1.001 \times 10^{-3} \text{ m}^3/\text{kg} = 1.001 \text{ cm}^3/\text{g},$$

and the molar volume is

$$V = \frac{2002 \times 10^{-3} \text{ m}^3}{2 \text{ kg}} \times \frac{18 \times 10^{-3} \text{ kg}}{\text{mol}} = 1.8018 \times 10^{-5} \frac{\text{m}^3}{\text{mol}} = 18.018 \frac{\text{cm}^3}{\text{mol}}.$$

In general for any extensive property F we have a corresponding intensive (specific or molar) property:

$$F_{\text{extensive}} = F_{\text{molar}} \times \text{(total number of moles)}$$
$$= F_{\text{specific}} \times \text{(total mass)}. \tag{1.3}$$

The relationship between specific and molar property is

$$F_{\text{molar}} = F_{\text{specific}} \cdot M_m, \qquad (1.4)$$

where M_m is the molar mass (kg/mol).

NOTE

Nomenclature

We will refer to properties like volume as extensive, with the understanding that they have an intensive variant. The symbol V will be used for the intensive variant, whether molar or specific. The total volume occupied by n mole (or m mass) of material will be written as V^{tot} , nV, or mV. No separate notation will be used to distinguish molar from specific properties. This distinction will be made clear by the context of the calculation.

State of Pure Component

Experience teaches that if we fix temperature and pressure, all other intensive properties of a pure component (density, heat capacity, dielectric constant, etc.) are fixed. We express this by saying that the state of a pure substance is fully specified by temperature and pressure. For the molar volume V, for example, we write

$$V = V(T, P), \tag{1.5}$$

which reads "V is a function of T and P." The term *state function* will be used as a synonym for "thermodynamic property." If eq. (1.5) is solved for temperature, we obtain an equation of the form

$$T = T(P, V), \tag{1.6}$$

which reads "T is a function of P and V." It is possible then to define the state using pressure and molar volume as the defining variables, since knowing pressure and volume allows us to calculate temperature. Because all properties are related to pressure and temperature, the state may be defined by any combination of two intensive variables, not necessarily T and P. Temperature and pressure are the preferred choice, as both variables are easy to measure and control in the laboratory and in an industrial setting. Nonetheless, we will occasionally consider different sets of variables, if this proves convenient.

NOTE

Fixing the State

If two intensive properties are known, the state of single-phase pure fluid is fixed, i.e., all other intensive properties have fixed values and can be obtained either from tables or by calculation.

State of Multicomponent Mixture The state of a multicomponent mixture requires the specification of *composition* in addition to temperature and pressure. Mixtures will be introduced in Chapter 8. Until then the focus will be on single components.

Process and Path

The thermodynamic plane of pure substance is represented by two axes, T and P. A point on this plane represents a state, its coordinates corresponding to the temperature and pressure of the system. The typical problem in thermodynamics involves a system undergoing a change of state: a fixed amount of material at temperature T_A and pressure P_A is subjected to heating/cooling, compression/expansion, or other treatments to final state (T_C, P_C) . A change of state is called a *process*. On the thermodynamic plane, a process is depicted by a *path*, namely, a line of successive states that connect the initial and final state (see Figure 1-6). Conversely, any line on this plane represents a process that can be realized experimentally. Two processes that are represented by simple paths on the TP plane are the constant-pressure (or isobaric) process is a straight line drawn at constant pressure (path AB in Figure 1-6); the constant-temperature process is drawn at constant temperature (path BC). Any two points on the TP plane can be connected using a sequence of isothermal and isobaric paths.

Processes such as the constant-pressure, constant-temperature, and constantvolume process are called *elementary*. These are represented by simple paths during which one state variable (pressure, temperature, volume) is held constant. They



Figure 1-6: Illustration of two different paths (ABC, AB'C) between the same initial (A) and final (C) states. Paths can be visualized as processes (heating/cooling, compression/expansion) that take place inside a cylinder fitted with a piston.

are also simple to conduct experimentally. One way to do this is using a cylinder fitted with a piston. By fitting the piston with enough weights we can exert any pressure on the contents of the cylinder, and by making the piston movable we allow changes of volume due to heating/cooling to take place while keeping the pressure inside the cylinder constant. To conduct an isothermal process we employ the notion of a *heat bath*, or heat reservoir. Normally, when a hot system is used to supply heat to a colder one, its temperature drops as a result of the transfer of heat. If we imagine the size of the hot system to approach infinity, any finite transfer of heat to (or from) another system represents an infinitesimal change for the large system and does not change its temperature by any appreciable amount. The ambient air is a practical example of a heat bath with respect to small exchanges of heat. A campfire, for example, though locally hot, has negligible effect on the temperature of the air above the campsite. The rising sun, on the other hand, changes the air temperature appreciably. Therefore, the notion of an "infinite" bath must be understood as relative to the amount of heat that is exchanged. A constanttemperature process may be conducted by placing the system into contact with a heat bath. Additionally, the process must be conducted in small steps to allow for continuous thermal equilibration. The constant-volume process requires that the volume occupied by the system remain constant. This can be easily accomplished by confining an amount of substance in a rigid vessel that is completely filled. Finally, the adiabatic process may be conducted by placing thermal insulation around the system to prevent the exchange of heat.

We will employ cylinder-and-piston arrangement primarily as a mental device that allows us to visualize the mathematical abstraction of a path as a physical process that we could conduct in the laboratory.

Quasi-Static Process

At equilibrium, pressure and temperature are uniform throughout the system. This ensures a well-defined state in which, the system is characterized by a single temperature and single pressure, and represented by a single point on the PT plane. If we subject the system to a process, for example, heating by placing it into contact with a hot source, the system will be temporarily moved away from equilibrium and will develop a temperature gradient that induces the necessary transfer of heat. If the process involves compression or expansion, a pressure gradient develops that moves the system and its boundaries in the desired direction. During a process the system is not in equilibrium and the presence of gradients implies that its state cannot be characterized by a single temperature and pressure. This introduces an inconsistency in our depiction of processes as paths on the TP plane, since points on this plane represent equilibrium states of well-defined pressure and temperature. We resolve this difficulty by requiring the process to take place in a special way, such that the displacement of the system from equilibrium is *infinitesimally* small. A process conducted in such manner is called *quasi static*. Suppose we want to increase the temperature of the system from T_1 to T_2 . Rather than contacting the system with a bath at temperature T_2 , we use a bath at temperature $T_1 + \delta T$, where δT is a small number, and let the system equilibrate with the bath. This ensures that the temperature of the system is nearly uniform (Fig. 1-7). Once the system is equilibrated to temperature $T_1 + \delta T$, we place it into thermal contact with another bath at temperature $T_2 + 2\delta T$, and repeat the process until the final desired temperature is reached. Changes in pressure are conducted in the same manner. In general, in a quasi-static process we apply small changes at a time and wait between changes for the system to equilibrate. The name derives from the Latin quasi ("almost") and implies that the process occurs as if the system remained at a stationary equilibrium state.

Quasi Static is Reversible A process that is conducted in quasi-static manner is essentially at equilibrium at every step along the way. This implies that the system can retrace its path if all inputs (temperature and pressure differences) reverse sign. For this reason, the quasi-static process is also a *reversible* process. If a process is conducted under large gradients of pressure and temperature, it is neither quasi static nor reversible. Here is an exaggerated example that demonstrates this fact. If an inflated balloon is punctured with a sharp needle, the air in the balloon will escape and expand to the conditions of the ambient air. This process is *not* quasi static because expansion occurs under a nonzero pressure difference between the air in the balloon back to the inflated state by reversing the action that led to the expansion, i.e., by "de-puncturing" it. We can certainly restore the initial state by patching the balloon and blowing air into it, but this amounts to performing an entirely different process. The same is true in heat transfer. If two systems



Figure 1-7: (a) Typical temperature gradient in heat transfer. (b) Heat transfer under small temperature difference. (c) Quasi-static idealization: temperatures in each system are nearly uniform and almost equal to each other.

exchange heat under a finite (nonzero) temperature difference, as in Figure 1-7(a), reversing ΔT is not sufficient to cause heat to flow in the reverse direction because the temperature gradient inside system 1 continues to transfer heat in the original direction. For a certain period of time the left side of system 1 will continue to receive heat until the gradient adjusts to the new temperature of system 2. Only when a process is conducted reversibly is it possible to recover the initial state by exactly retracing the forward path in the reverse direction. The quasi-static way to expand the gas is to perform the process against an external pressure that resists the expansion and absorbs all of the work done by the expanding gas. To move in the forward direction, the external pressure would have to be slightly lower than that of the gas; to move in the reverse direction, it would have to be slightly higher. In this manner the process, whether expansion or compression, is reversible. The terms quasi static and reversible are equivalent but not synonymous. Quasi static refers to how the process is conducted (under infinitesimal gradients); reversible refers to the characteristic property that such process can retrace its path exactly. The two terms are equivalent in the sense that if we determine that a process is conducted in a quasi-static manner we may conclude that it is reversible, and vice versa. In practice, therefore, the two terms may be used interchangeably.

NOTE

About the Quasi-Static Process

The quasi-static process is an idealization that allows us to associate a path drawn on the thermodynamic plane with an actual process. It is a mental device that we use to draw connections between mathematical operations on the thermodynamic plane and real processes that can be conducted experimentally. Since this is a mental exercise, we are not concerned as to whether this is a practical way to run the process. In fact, this is a rather impractical way of doing things: Gradients are desirable because they increase the rate of a process and decrease the time it takes to perform the task. This does not mean that the quasi-static concept is irrelevant in real life. When mathematics calls for an infinitesimal change, nature is satisfied with a change that is "small enough." If an actual process is conducted in a way that does not upset the equilibrium state too much, it can then be treated as a quasi-static process.

Example 1.3: The Cost of Doing Things Fast

You want to carry a cup of water from the first floor to your room on the second floor, 15 feet up. How much work is required?

Solution A cup holds about 250 ml, or 0.25 kg of water. The potential energy difference between the first and second floor is

 $\Delta E_p = mgh = (0.25 \text{ kg})(9.81 \text{ m/s}^2)(15 \text{ ft})(0.3048 \text{ m/ft}) = 11.2 \text{ J}.$

Therefore, the required amount of work is 11.2 J—but only if the process is conducted in a quasi-static way! Picture yourself hurrying up the stairs: The surface of the liquid is not level but forms ripples that oscillate. The liquid might even spill if you are a little careless, by jumping over the brim. This motion of the liquid takes energy that was not accounted for in the previous calculation. By the time you reach your room you will have consumed more than 11.2 J. Suppose you want to recover the work you just spent. You could do this by dropping the glass to the first floor onto some mechanical device with springs and other mechanical contraptions designed to capture this work. However, you will only be able to recover the 11.2 J of potential energy. The additional amount that went into producing the ripples will be unavailable. This energy is not lost; it is turned into internal energy, as we will see in Chapter 3. You can still extract it, but this will require more work than the amount you will recover, as we will learn in Chapter 4.

Here is the quasi-static way to conduct this process: Take small, careful steps, trying to avoid getting the liquid off its level position. That way the liquid will always stay level (in equilibrium) and the amount of work you will do will exactly match the calculation. Of course, this will take more time, but it will require no more than the theoretical work. The point is that, doing things in a nonquasi-static manner is fast but also carries a hidden cost in terms of extra work associated with the presence of gradients and nonequilibrium states. Doing things in a quasi-static manner is inconvenient, but more efficient, because it does not include any hidden costs.

1.4 Units

Throughout this book we will use primarily the SI system of units with occasional use of the American Engineering system. The main quantities of interests are pressure, temperature, and energy. These are briefly reviewed below. Various physical constants that are commonly used in thermodynamics are shown in Table 1-1.

Pressure Pressure is the ratio of the force acting normal to a surface, divided by the area of the surface. In thermodynamics, pressure generates the forces that give

Avogadro's number	$N_{\rm A} = 6.022 \times 10^{23} \ {\rm mol}^{-1}$
Boltzmann's constant	$k_B = 1.38 \times 10^{-23} \text{ J/K}$
Ideal-gas constant	$R = k_B N_{\rm A} = 8.314 \text{ J/mol K}$
Absolute zero	0 K = 0 R = -273.15 °C = -459.67 °F

rise to mechanical work. The SI unit of pressure is the pascal, Pa, and is defined as the pressure generated by 1 N (newton) acting on a 1 m^2 area:

$$Pa = \frac{N}{m^2} = \frac{J}{m^3}.$$
(1.7)

The last equality in the far right is obtained by writing $J = N \cdot m$. The pascal is an impractically small unit of pressure because 1 N is a small force and 1 m² is a large area. A commonly used multiple of Pa is the bar:

$$1 \text{ bar} = 10^5 \text{ Pa} = 100 \text{ kPa} = 0.1 \text{ MPa}.$$
 (1.8)

An older unit of pressure, still in use, is the Torr, or mm Hg, representing the hydrostatic pressure exerted by a column of mercury 1 mm high. In the American Engineering system of units, pressure is measured in pounds of force per square inch, or psi. The relationship between the various units can be expressed through their relationship to the standard atmospheric pressure:

$$1 \text{ atm} = \begin{cases} 1.013 \text{ bar} = 1.013 \times 10^5 \text{ Pa} \\ 760 \text{ Torr} = 760 \text{ mm Hg} \\ 14.696 \text{ psi} \end{cases}$$
(1.9)

Temperature Temperature is a fundamental property in thermodynamics. It is a measure of the kinetic energy of molecules and gives rise the sensation of "hot" and "cold." It is measured using a thermometer, a device that obtains temperature indirectly by measuring some property that is a sensitive function of temperature, for example, the volume of mercury inside a capillary (mercury thermometer), the electric current between two different metallic wires (thermocouple), etc. In the SI system, the absolute temperature is a fundamental quantity (dimension) and its unit is the kelvin (K). In the American Engineering system, absolute temperature is measured in rankine (R), whose relationship to the kelvin is,

$$1 \text{ K} = 1.8 \text{ R.}$$
 (1.10)

Temperatures measured in absolute units are always positive. The absolute zero is a special temperature that cannot be reached except in a limiting sense.

In practice, temperature is usually measured in empirical scales that were originally developed before the precise notion of temperature was clear. The two most widely used are the Celsius scale and the Fahrenheit. They are related to each other and to the absolute scales as follows:⁴

$$\frac{T}{^{\circ}\mathrm{F}} = 1.8 \frac{T}{^{\circ}\mathrm{C}} + 32$$
 (1.11)

^{4.} The notation $T/^{\circ}C$ reads, "numerical value of temperature expressed in °C." For example, if T = 25 °C, then $T/^{\circ}C$ is 25.

$$\frac{T}{K} = \frac{T}{^{\circ}C} + 273.15 \tag{1.12}$$

$$\frac{T}{R} = \frac{T}{^{\circ}F} + 459.67, \qquad (1.13)$$

where the subscript in T indicates the corresponding units. The units of absolute temperature are indicated without the degree (°) symbol, for example, K or R; the units in the Celsius and Fahrenheit scales include the degree (°) symbol, for example, °C, °F. Although temperatures are almost always measured in the empirical scales Celsius or Fahrenheit, it is the absolute temperature that must be used in all thermodynamics equations.

Mole (mol, gmol, lb-mol) The mole⁵ is a defined unit in the SI system such that 1 mol is an amount of matter that contains exactly $N_{\rm A}$ molecules, where $N_{\rm A} = 6.022 \times 10^{23} \text{ mol}^{-1}$ is Avogadro's number.⁶ The mass of 1 mol is the *molar mass* and is numerically equal to the molecular weight multiplied by 10^{-3} kg. For example, the molar mass of water (molecular weight 18.015) is

$$M_m = 18.015 \times 10^{-3} \text{ kg/mol.}$$
 (1.14)

The symbol M_m will be used to indicate the molar mass. The number of moles n that correspond to mass m is

$$n = \frac{m}{M_m}.$$
(1.15)

The pound-mol (lb-mol) is the analogous unit in the American Engineering system and represents an amount of matter equal to the molecular weight expressed in lbm. The relationship between the mol and lb-mol is

$$1 \text{ lb-mol} = 454 \text{ mol.}$$
 (1.16)

Energy The SI unit of energy is the joule, defined as the work done by a force 1 N over a distance of 1 m, also equal to the kinetic energy of a mass 1 kg with velocity 1 m/s:

$$\mathbf{J} = \mathbf{N} \cdot \mathbf{m} = \frac{\mathrm{kg} \cdot \mathbf{m}^2}{\mathrm{s}^2}.$$
 (1.17)

The kJ (1 kJ = 1000 J) is a commonly used multiple.

As a form of energy, heat does not require its own units. Nonetheless, units specific to heat remain in wide use today, even though they are redundant and

^{5.} The symbol of the unit is "mol" but the name of the unit is "mole," much like the unit of SI temperature is the kelvin but the symbol is K.

^{6.} The units for Avogadro's number are number of molecules/mol, and since the number of molecules is dimensionless, 1/mol.

require additional conversions when the calculation involves both heat and work. These units are the cal (calorie) and the Btu (British thermal unit) and are related to the joule through the following relationships:

$$cal = 4.18 J = 4.18 \times 10^{-3} kJ$$
 (1.18)

Btu =
$$1.055 \times 10^{-3}$$
J = 1.055 kJ. (1.19)

Some unit conversions encountered in thermodynamics are shown in Table 1-2.

Magnitude	Definition	Units	Other Units and Multiples
Length	_	m	$1 \text{ cm} = 10^{-2} \text{ m}$
			1 ft = 0.3048 m
			1 in = 2.54×10^{-2} m
Mass	_	kg	$1 \text{ g} = 10^{-3} \text{ kg}$
			1 lb = 0.4536 kg
Time	_	S	$1 \min = 60 \mathrm{s}$
			1 hr = 3600 s
Volume	$(length)^3$	m^3	$1 \text{ cm}^3 = 10^{-6} \text{ m}^3$
			$1 L = 10^{-3} m^3$
Force	$(mass) \times (acceleration)$	${\rm N}={\rm kg}\;{\rm m}\;{\rm s}^{-2}$	1 lbf = 4.4482 N
Pressure	(force)/(area)	$Pa = N m^{-2}$	$1 \text{ Pa} = 10^{-3} \text{ kJ/m}^3$
	= (energy)/(volume)		$1 \text{ bar} = 10^5 \text{ Pa}$
			1 psi = 0.06895 bar
Energy	$(force) \times (length)$	$\mathrm{J} = \mathrm{kg} \ \mathrm{m}^2 \ \mathrm{s}^{-2}$	$1 \text{ kJ} = 10^3 \text{ J}$
	$= (mass) \times (velocity)^2$		1 Btu = 1.055 kJ
Specific energy	(energy)/(mass)	J/kg	1 kJ/kg=2.3237 kJ/kg
			1 Btu/lbm=2.3237 kJ/kg
Power	(energy)/(time)	W = J/s	1 Btu/s = 1.055 kW
			1 hp = 735.49 W

Table 1-2: Common units and conversion factors

1.5 Summary

Thermodynamics arises from the physical interaction between molecules. This interaction gives rise to temperature as a state variable, which, along with pressure, fully specifies the thermodynamic state of a pure substance. Given pressure and temperature, all intensive properties of a pure substance are fixed. This means that we can measure them once and tabulate them as a function of pressure and temperature for future use. Such tabulations exist for many substances over a wide range of conditions. Nonetheless, for engineering calculations it is convenient to express properties as mathematical functions of pressure and temperature. This eliminates the need for new experimental measurements—and all the costs associated with raw materials and human resources—each time a property is needed at conditions that are not available from tables. One goal of chemical engineering thermodynamics is to provide rigorous methodologies for developing such equations.

Strictly speaking, thermodynamics applies to systems in equilibrium. When we refer to the pressure and temperature of a system we imply that the system is in equilibrium so that it is characterized by a single (uniform) value of pressure and temperature. Thermodynamics also applies rigorously to quasi-static processes, which allow the system to maintain a state of almost undisturbed equilibrium throughout the entire process.

1.6 Problems

Problem 1.1: The density of liquid ammonia (NH₃) at 0 °F, 31 psi, is 41.3 lb/ft³. a) Calculate the specific volume in ft³/lb, cm³/g and m³/kg.

b) Calculate the molar volume in $ft^3/lbmol$, cm^3/mol and m^3/mol .

Problem 1.2: The equation below gives the boiling temperature of isopropanol as a function of pressure:

$$T = \frac{B}{A - \log_{10} P} - C,$$

where T is in kelvin, P is in bar, and the parameters A, B, and C are

$$A = 4.57795, \quad B = 1221.423, \quad C = -87.474.$$

Obtain an equation that gives the boiling temperature in ${}^{\circ}F$, as a function of $\ln P$, with P in psi. *Hint:* The equation is of the form

$$T = \frac{B'}{A' - \ln P} - C'$$

but the constants A', B', and C' have different values from those given above.

Problem 1.3: a) At 0.01 °C, 611.73 Pa, water coexists in three phases, liquid, solid (ice), and vapor. Calculate the mean thermal velocity (\bar{v}) in each of the three phases in m/s, km/hr and miles per hour.

b) Calculate the mean translational kinetic energy contained in 1 kg of ice, 1 kg of liquid water, and 1 kg of water vapor at the triple point.

c) Calculate the mean translational kinetic energy of an oxygen molecule in air at 0.01 $^{\circ}\mathrm{C},$ 1 bar.

Problem 1.4: The intermolecular potential of methane is given by the following equation:

$$\Phi(r) = a \left[\left(\frac{\sigma}{r}\right)^{12} - \left(\frac{\sigma}{r}\right)^6 \right]$$

with $a = 2.05482 \times 10^{-21}$ J, $\sigma = 3.786$ Å, and r is the distance between molecules (in Å).

a) Make a plot of this potential in the range r = 3 Å to 10 Å.

b) Calculate the distance r_* (in Å) where the potential has a minimum.

c) Estimate the density of liquid methane based on this potential.

Find the density of liquid methane in a handbook and compare your answer to the tabulated value.

Problem 1.5: a) Estimate the mean distance between molecules in liquid water. Assume for simplicity that molecules sit on a regular square lattice.

b) Repeat for steam at 1 bar, 200 °C (density $4.6\times10^{-4}~{\rm g/cm^3}).$ Report the results in Å.

Problem 1.6: In 1656, Otto von Guericke of Magdeburg presented his invention, a vacuum pump, through a demonstration that became a popular sensation. A metal sphere made of two hemispheres (now known as the Magdeburg hemispheres) was evacuated, so that a vacuum would hold the two pieces together. Von Guericke

would then have several horses (by one account, 30 of them, in two teams of 15) pulling, unsuccessfully, to separate the hemispheres. The demonstration would end with the opening of a valve that removed the vacuum and allowed the hemispheres to separate. Suppose that the diameter of the sphere is 50 cm and the sphere is completely evacuated. The sphere is hung from the ceiling and you pull the other half with the force of your body weight. Will the hemispheres come apart? Support your answer with calculations.

Index

Note: page numbers with "f" indicate figures; those with "t" indicate tables.

Absolute temperature, 23–24 Absolute zero, 22t Accumulation, 253 Acentric factor, 47–51 defined, 47-48 of simple, normal, and polar fluids, 50-51 Activity, 606–13 chemical potential and, 607 of gas, 607-8, 611 of liquid, 608-9, 611 P° , working with, 608 of solid, 609-10, 612 of solute, 609, 611-12 standard state and, 610, 613 Activity coefficient, 504–11 for data reduction, 512–15 defined. 504 deviations from Raoult's law, 508–10, 509f experimental, 510–15 Gibbs free energy and, excess, 505–7, 510-14, 511f limits of, 505 phase equilibrium and, 507-10 solubility limits using, 547-48 usefulness of, 505 Activity coefficient models, 515–31 Flory-Huggins, 521–22 Margules, 515-19 NRTL, 520-21 UNIFAC, 525-31 UNIQUAC, 522-25 vanLaar, 519 Wilson, 519-20 Adiabatic flame temperature, 605–6 Adiabatic mixing heat effects of, 497-99 of solutions on enthalpy charts, 503f in steady-state processes, 276–78, 277f Adiabatic processes. See Reversible adiabatic processes Adiabatic production of work, 261, 262 Adiabatic system, 13 Air, chemical potential in, 441–42

American Engineering system of units, 22 pound-mol (lb-mol) in, 24 pressure measured in, 23 temperature measured in, 23 Ammonia refrigerator, 304–6 Analogous relationships, 215, 408 Antoine equation, 38–40 Clausius-Clapeyron equation and, 343 determining phase with, 39–40 units in, 38-39 ASHRAE designation of refrigerants, 307t Athermal process of mixing, 410 Avogadro's number, 22t Azeotropes, 380-81, 380f Balances in open systems, 251–335 energy balance, 254f, 255-58 entropy balance, 258-66 flow streams, 252–53, 252f liquefaction, 309–15 mass balance, 253–55, 254f power generation, 295–300 problems, 324-35 refrigeration, 301–9 summary, 323-24 thermodynamics of steady-state processes, 272 - 94unsteady-state balances, 315-23 Bar, 23 Bath change of, entropy, 159-61 default, exergy and, 189-91 heat, in entropy balance, 265–66 stream acting as, in entropy balance, 264-65 Benedict-Webb-Rubin equation, 67–71, 70f, 71t Benzene, solubility of, 577–78, 578f Binary mixtures, 420–21, 423t Binary VLE using Soave-Redlich-Kwong, 452 - 53Boltzmann constant, 8, 22t Bubble temperature (or point), 371 BWR equation. See Benedict-Webb-Rubin equation

Calorie, 101 Carbon dioxide (CO_2) density of liquid, 10 ideal-gas state and, 10-11 intermolecular potential of, 6 Pxy graph of CO_2/n -pentane calculated using Soave-Redlich-Kwong, 451f, 452-53 Carnot cycle, 168–77 defined, 169 in entropy, 168-77, 169f first-law analysis of, 170 ideal gas used in, 173-74 internal combustion engine example of, 173second-law analysis of, 171 steam used in, 175-76 steps in, 169-70 thermodynamic efficiency of, 171-73 on TS graph, 169f work value of heat and, 182-83, 182f Carnot efficiency, 171-72 Celsius scale, 23–24 Chemical engineer, 5 Chemical engineering thermodynamics, 5 Chemical equilibrium, 15 Chemical potential activity and, 607 in air, 441-42 in fugacity, 444 in Gibbs free energy, 440–42 in ideal-gas state, 440 in real mixture, 440 in theory of VLE, 439–42 Chemical thermodynamics, 3-5, 4f Classical thermodynamics laws of, 11–12 vs. statistical thermodynamics, 11-13 Clausius, Rudolph, 178 Clausius-Clapeyron equation in VLE, 341–43 Clausius statement as alternative statement of second law, 177 - 82defined, 178 as equivalent statement of second law, 180 - 82Closed systems defined, 13 first law for, 98–101 second law in, 150-53 Combinatorial molecular interactions, 507 Completely immiscible liquids, 558–61 calculations, limitations of, 563 Pxy graph of, 561-62, 562f Txy graph of, 559-61, 559f Composite system, 13

Compressed liquids, 292–94 entropy of, 156 Poynting equation for calculating, 345–47 throttling of, 288-89, 290f Compressibility factor, 43–45, 45f in BWR equation, 69 in corresponding states, 45-47, 46f, 51, 52 in Lee-Kesler method, 56, 68 in Peng-Robinson equation, 67 in Pitzer method, 48, 71 in Rackett equation, 73 roots in, acceptable, 63, 66, 67 in Soave-Redlich-Kwong equation of state, 61in van der Waals equation, 58-60 in virial equation, 53, 54, 56 ZP graph of pure fluids and, 43–45, 45f, 56 Compressor graphical solution on Molliev chart, 293f steam/gas, 290–92 Condensed phases, 9 Constant composition, systems of, 407–8 Constant-pressure cooling, 104–5 Constant pressure entropy change at, 155 no phase change in, 153–54 Constant-pressure heat capacity (C_P) , 111–12 vs. constant-volume heat capacity, 111-12, 112f as state function, 113 of steam, 114-15 Constant-pressure heating, 102–3 Constant-pressure (or isobaric) process, 18–19 Constants, 22t Constant-temperature (or isothermal) process, 18-19, 107, 108 Constant-volume cooling, 102 Constant-volume heat capacity (C_V) , 109 vs. constant-pressure heat capacity, 111–12, 112f as state function, 113 Constant-volume heating, 101-2 Constant-volume path entropy, no phase change in, 154 Constant-volume process, 18–19 Constrained equilibrium, 15–16 Conversions, 25t Corresponding states in compressibility factor, 45-47, 46f, 51, 52 in phase diagrams of pure fluids, 45, 46f Cubic equations of state application to, 230-34 fugacity calculated from, 352-53 isotherm, unstable and metastable parts of, 62 - 63

Peng-Robinson, 61, 66-67 PVT behavior of, 61–63 roots of, 63-65 Soave-Redlich-Kwong, 30f, 60-61, 66 of state, residual properties from, 232t Van der Waals, 58-60, 65-66 for volume, solving, 65–67 working with, 64 Data reduction, 514 Definitions, 13–17 equilibrium, 15–16 property, 16-17 system, 13-14 Density empirical equations for, 72-77 of liquid CO_2 , 10 Derivatives with functions of multiple variables, 110 Desalination, 585–86 Dew point, 483 Diathermal system, 13 Differentials exact, 211-12 form of, 209-11 inexact, 212 integration of, 213-14, 214f Diffusion in osmotic equilibrium, 582–83 Disorder, defined, 196 Distillation, 378, 379f Double interpolations, 41, 41f, 42 Elementary process, 18-19 Empirical equations, 57 for density, 72-77 summary, 78 Endothermic process, 410 Energy, 24–25, 25t forms of, 90 heat and, 96-97 ideal-gas state, 124–32 internal, 96 process requirements, calculating, 5 storable, 89 transfer, sign convention for direction of, 89 work and, 88-89, 88f Energy balance, 254f, 255–58 in closed systems, 257–58 in enthalpy of vaporization, 478–79 entropy used in, 163-66 in heat exchanger, 479-80 in ideal solution, 475–80 irreversible processes and, 133–38 in open systems, 254f, 255-58

steady state, 258 using C_P and $\Delta H_{\rm vap}$, 122–24 using tables, 121–22 Energy balances in reacting systems, 601–6 adiabatic flame temperature and, 605-6 heat of combustion and, 603–5 setup for energy balance of reactor, 602f Enthalpy defined, 103 enthalpy-entropy (Mollier) chart, 244–45, 245fequations for, 217–19 excess, heat effects of mixing and, 496, 497f ideal-gas, 234 of ideal-gas mixture, 416 lever rule for, 119-20 of mixing, 425 pressure and temperature effect on, 220–22 pressure-explicit relations, 229 of reactions, standard, 596-601, 599f residual, 223, 236, 237f as state function, 103, 125-26of steam, 103-5 temperature-enthalpy chart, 243-44, 244f of vaporization, 478–79 Enthalpy charts, 500–504 adiabatic mixing of solutions on, 503f of hydrazine/water mixtures, 501f pressure, 242–43, 243f using, 503-4 Enthalpy-entropy (Mollier) chart, 244-45, 245f graphical solution of compressed liquids on, 293f in steam turbine, 285-86, 285f Entropy calculation of (See Entropy, calculation of) Carnot cycle in, 168–77, 169f change of bath, 159-61 in energy balance, 163–66 energy balances using, 163-66 equations for, 217-19 equilibrium and, 191–95 exergy and, 189–91 generation, 167-68 heat calculated using, 166 ideal-gas, 234 of ideal-gas mixture, 416 ideal work in, 183-88 of irreversibility, 168 of liquids, 156, 157 lost work in, 183–88, 191 measurable quantities relating to, 151–53 of mixing, in ideal solution, 463–64 molecular view of, 195-99, 197f pressure and temperature's effect on, 220-22

Entropy (*Continued*) pressure-explicit relations, 229-30 problems, 201-4 residual, 224, 236, 238f reversibility and, 176-77 second law and, 149–204 of solids, 155-56, 157 stability and, 191-95 as state function, 153 summary, 199-201 temperature and, 153 thermodynamic potentials, 194–95 of universe, 168 of vaporization, 157, 158 Entropy, calculation of, 153–63, 199 basic formula, 154 change at constant pressure, 155 change of bath, 159-61 compressed liquids, 156 constant-pressure path, no phase change, 153 - 54constant-volume path, no phase change, 154 energy balances with phase change, using C_P and $\Delta H_{\rm vap}$, 158–59 ideal-gas state, 161-62, 161f phase change, 157-58, 157f solids, 155-56 steam, 163 tabulated values used for, 162 vaporization, 158 Entropy balance, 258–66 heat exchange between streams, 262-63 in open systems, 258–66 processes with entropy generation, 262f reversible adiabatic process, 260–61 steady state, 260, 261 stream acting as a bath, 264–65 Entropy generation cooling system, choosing, 269–71 in power plant, 267 processes with, 262f Equations of state appeal of, 453 binary VLE using Soave-Redlich-Kwong, 452 - 53BWR, 67-71, 70f, 71t in compressibility factor, 44 cubic, 57-67 defined, 29 fugacity from, 446-48 Henry's law from, 572–73 ideal-gas law and, 34, 54 interaction parameter, 451–53 Lee-Kesler, 68-70

mathematical representation of, 44 for mixtures, 419-21 other, 67-71 phase diagrams from, 356–58 Pitzer, 71 properties from mixtures, 421–27 saturation pressure from, 353-56 summary, 77 in theory of VLE, 448-53 in truncated virial equation, 54 Equilibrium, 15-16, 545-91. See also Liquid miscibility chemical, 15 conditions at constant temperature and pressure, 191–94 conditions fulfilled by, 15 constrained, 15–16 entropy and, 191–95 gas liquids, solubility of, 561-74 liquid-liquid (LLE), 369 liquid-liquid-vapor (LLVE), 369 mechanical, 15 osmotic, 580-86 phase splitting and Gibbs free energy, 548 - 56problems, 586–91 schematic of, 546f solids in liquids, solubility of, 575-80 solids involved in, 629–32 vs. steady state, 261 summary, 586 thermal, 15 thermodynamic potentials and, 194–95 Equilibrium composition, 622–24 with multiple reactions, 634–35 pressure in, effect of, 623–24 Equilibrium constant, 614–20, 621 Ethylene, phase diagram of, 356–58 Euler's theorem, 406 Eutectic point, 579–80 Exact differential, 211–12 Excess properties, 489–96 as mathematical operator, 490 molar, 490-91, 492f in nonideal solutions, 489–96 Redlich-Kister expansion, 495–96 volume, 494-95, 495f in volume of mixing, 492–94 Exergy, 189-91 Exothermic process, 410 Expansion, PV work in, 92-93Expansion and Compression of Liquids, 292 - 94Experimental activity coefficient, 510–15 fitting, 512-14

Pxy graph of, 515f Extensive property, 16–17 Fahrenheit, 23–24 First law Carnot cycle analyzed by, 170 for closed system, 98-101 defined, 87 energy and, 87-148 history of, 100-101 Joule's experiment, 100–101 operator Δ used in, 99–100 paths in, 101-8 problems, 140-48 schematic illustration of, 98f summary, 139-40 Fixed property, 17 Flash separation, 375–76, 376f Flash units, multiple, 377-78 Flory-Huggins equation, 521–22 Flow streams, 252–53, 252f Force, 25t Fugacity, 343–53 chemical potential and, 444 defined, 343-43 from equations of state, 446–48 from experimental data, 445 Gibbs free energy and, 344–45 Henry's law used to calculate, 573–74, 574f in ideal-gas state, 344 in ideal solution, 464–65 Lewis-Randall rule used to calculate, 471, 563, 564 in mixture using Soave-Redlich-Kwong, 447 - 48of solubility of gases in liquids, 564f steam, 349 from steam tables, 347 in theory of VLE, 443-48 Fugacity, calculation of, 345-53 compressibility factor used in, 348-49 from cubic equations of state, 352–53 from generalized graphs, 349-52, 350f, 351f Poynting equation for compressed liquids, 345 - 47saturated liquid, 346 from Soave-Redlich-Kwong, 352, 353 tabulated properties used in, 347–48 Function, differential and integral forms of, 209 - 11Fundamental relationships calculating, 214–17 change of variables, 217 summary of, 216t

Gas activity of, 607-8, 611 Linde process for liquefaction of, 310f Gases in liquids, solubility of, 563–74. See also Henry's law fugate of, 564f Generalized correlations, calculating, 235–36, 237-38f Generalized graphs, 77 fugacity calculated from, 349-52, 350f, 351f Gibbs, J. Willard, 4-5, 4f Gibbs-Duhem equation, 406–7, 439–40 Gibbs free energy, 5, 194–95, 195f calculating, 215, 225, 242 chemical potential in, 440–42 excess, activity coefficient and, 505-7, 510-14, 511f fugacity and, 344-45 in Margules equation, linearized form of excess, 518f multicomponent equilibrium in, 437-38, 437f phase rule in, 438–39 phase splitting and, 548–56 in theory of VLE, 435–39 Gibbs's phase rule, 438–39 Heat, 96-97 capacities, 109-19 of combustion in reacting systems, 603–5 direction of flow, second law to determine, 184 - 85entropy used to calculate, 166 as path function, 105-6 sensible, 109 sign convention for, 97 specific, 111 transfer, in entropy generation, 188 transfer, irreversible processes in, 133 of vaporization, 119–24, 120f of vaporization using Soave-Redlich-Kwong, 338 work and, shared characteristics with, 97 work value of, Carnot cycle and, 182–83, 182f Heat bath (or heat reservoir), 19 Heat capacity, 109–19 constant-pressure heat capacity, 111-12, 112f constant-volume heat capacity, 109, 111–12, 112f

defined, 112–13

effect of pressure and temperature on, 113–19, 113f

excess, 499--500

Heat effects of mixing, 496–504 enthalpies, excess, 496, 497f enthalpy charts, 500-504 excess heat capacity, 499-500 isothermal, 497–99 Heat exchanger, 278-81, 279f in ideal solution, 479–80 Heat of vaporization $(\Delta H_{\rm vap})$, 119–24, 120f C_P and $\Delta H_{\rm vap}$, energy balances with phase change using, 122–24 latent, 119 Pitzer correlation for, 121–22 tables, energy balances with phase change using, 121-22 Helmholtz free energy, 194, 216, 225, 242 Henry's law, 564-74 alternative forms of, 566-67 carbonated soda and, 571-72 from equation of state, 572-73 formal thermodynamics and, 569-70, 571f fugacity calculated with, 573-74, 574f vs. Lewis-Randall rule, 573–74 other units for, 565–66 in simultaneous dissolution of two gases, 567 - 69temperature and pressure effects on, 569 VLE using, 564–65 Household refrigerator, 304 Humidification, 481-83 dew point, 483 relative humidity, 482, 483 Hypothetical states, 476–77 Ideal gas filling a tank with, 318–18 throttling of, 288 venting, 322-23

Ideal-gas constant, 22t Ideal-gas law calculated isotherms using, 57f defined. 34 directions to, 34 equation of state and, 34, 54 molar volume calculated with, example of, 55summary, 78 vs. truncated viral equation, 54 Ideal-gas state, 10–11, 124–32 calculating, 219-20 Carnot cycle using, 173–75 chemical potential in, 440 equations, summary of, 219t fugacity in, 344 hypothetical, 223

irreversible expansion of, 137 in isothermal compression of steam, 126-27 $\log x mean, 130$ mixtures in, 413–19 paths in, 132f residual properties of, 225–26 reversible adiabatic compression of nitrogen, 131 - 32reversible adiabatic process, 127-30, 131-32, 132f reversible adiabatic process in, 164-66 triple-product rule in, 207 Ideal solution, 461–88 defined, 462 energy balances in, 475-80 entropy of mixing in, 463-64 fugacity in, 464-65 ideality in, 461-63 noncondensable gases in, 480–83 practical significance of, 463 problems, 484-88 in separation of work, 464 summary, 484 VLE in, Raoult's law, 466-74 Ideal work, 183-88 for heat transfer, 268-69 in open systems, 266-71 Incompressible phases, 220–21 Inexact differential, 212 Integral form of a function, 209–11 Integrals with functions of multiple variables, 110Integration of differentials, 213–14, 214f Integration paths, 109–10 Intensive property, 16–17 Interaction parameter, 451–53 Intermolecular potential, 6–7, 7f Internal energy, 96, 215, 219, 224-25, 241-42 Interpolations, 40–43, 41f accuracy in, 40 example of, using steam tables, 41-43 types of, 41f Irreversible processes, energy balances and adiabatic mixing, 134–36 heat transfer, 133 of ideal gas, 137 against pressure, 138 against vacuum, 136-37 Isentropic step in Carnot cycle, 170 Isolated system, 13 Isothermal compression of steam in first law paths, 108 in ideal-gas state, 126–27 in PV work, 94-95, 96f Isothermal mixing, heat effects of, 497–99

Index

Isothermal step in Carnot cycle, 169–70 Isotherms critical point and, 33 of Lee-Kesler method, 68 of modified BWR equation, 67, 70f pressure-volume, of acetone, 74-75, 76f on PV graph, 31, 33 of Soave-Redlich-Kwong equation, 61-62, 62f at zero pressure, 44 on ZP graph, 53, 57f Joule, James Prescott, 100–101 Kelvin (K), 23 Kelvin-Plank statement, 178 K-factors, 382, 449, 468 Kinetic energy, 90 Latent heat of vaporization, 119 Laws of classical thermodynamics, 11–12 Lee-Kesler method compressibility factor in, 56, 68 in phase diagrams of pure fluids, 48–49, 48f, 49f, 50f for residual enthalpy, 237f for residual entropy, 238f Length, 25t Lever rule, 34-36, 35f defined, 35 for enthalpy, 119-20 partially miscible liquids and, 388 in phase behavior of mixtures, 372–73 setup for application of, 35f state located with, steam table example, 43 using, reasons for, 36 Lewis-Randall rule defined, 565 fugacity in liquid phase given by, 471, 563, 564vs. Henry's law, 573-74 Linde process, 310f Linear interpolations, 41f, 71, 79 Liquefaction, 309–15 of gas, Linde process for, 310f of nitrogen, 310f, 311-14 Liquid-liquid equilibrium (LLE), 369, 546f Liquid-liquid-vapor equilibrium (LLVE), 369 Liquid miscibility complete, 558-61 partial, equilibrium between, 545-48 temperature and, 556-58 Liquids. See also Compressed liquids; Vapor-liquid mixture activity of, 608-9, 611

 CO_2 , density of, 10 constant-pressure cooling of, 115-17 of enthalpy and entropy, pressure and temperature's effect on, 220-22entropy of, 156, 157 expansion of, 292-94 fugacity of saturated, 346 gases in, solubility of, 563-74 heat capacities, 114 hypothetical state of, 472 properties, compressed, 117-19, 118f pump, calculating, 294 solids in, solubility of, 575–80 Log-x mean, 130 Lost work in open systems, 266–71 Magdeburg hemispheres, 27–28 Margules equation, 515–19 Gibbs free energy in, 518f Pxy graph reconstructed from limited data, 517.518-19 Mass. 25t Mass balance, 253-55, 254f Mathematical conditions for stability, 552 Maxwell-Boltzmann distribution, 8, 9f Maxwell relationships, 214, 216 Measurable quantities relating to entropy, 151 - 53Mechanical equilibrium, 15 Mechanically reversible process, 91–92, 92f Methane, virial coefficient used for residual properties of, 227–28 Mixing, 411–13. See also Mixtures athermal process of, 410 endothermic process of, 410 enthalpy of, 425 exothermic process of, 410 heat effects of, 496–504 molecular view of, 412f non-isothermal, 416–18 properties of, 409–11 rules, 419 separation and, 411–13 separation of air, 418–91 volume of, 409–10 volume of, excess properties in, 492–95 Mixtures, 401–33. See also Mixing binary, 420–21 composition of, 402-4 equations of state for, 419-21 formation of, at constant pressure and temperature, 410f fugacity in, using Soave-Redlich-Kwong, 447 - 48

Mixtures (*Continued*) homogeneous properties of, 403-4 in ideal-gas state, 413-19 mathematical treatment of, 404–9 phase behavior of. 369-400 problems, 428-33 properties from equations of state, 421–27 real, compression of, 427 real, properties of, 424-25 residual properties of, 420, 421 subscripts, 411 summary, 428 VLE of, using equations of state, 448–53 Mixtures, mathematical treatment of, 404-9 Euler's theorem, 406 Gibbs-Duhem equation, 406-7 partial molar property, 405, 408-8 systems of constant composition, 407–8 Molar mass, 23 Molar property, 16–17 excess, in nonideal solutions, 490-91, 492f partial, 405, 408-9 residual, 408-9 residual partial, 408-9 Molar volume of compressed liquid, 73 in compressibility factor, 44 in corresponding states, 51, 52 in cubic equations, 64, 65, 66, 67 ideal-gas, 55 liquid, in Rackett equation, 72–73 mean intermolecular distance and, 29 proper, selecting, 63 in PT graph of pure fluid, 37, 37f in PV graph of pure fluid, 30f, 31–35 in PVT behavior of pure fluid, 29–30 in Soave-Redlich-Kwong equation, 62 in van der Waals equation, 59 in virial equation, 55, 56 Mole, 24 Molecular basis of thermodynamics, 5–11 condensed phases, 9 density of liquid CO_2 , 10 ideal-gas state, 10–11 intermolecular potential, 6–7, 7f Maxwell-Boltzmann distribution, 8, 9f phase transitions, 8–9 temperature and pressure, 7–8 Molecular collisions, 7-8, 97 Molecular view of entropy, 195–99, 197f equally probable microstates, 199 probabilities and, 198–99 Mollier chart. See Enthalpy-entropy (Mollier) chart

Multicomponent mixture, state of, 18 Multiple reactions, 632–35 equilibrium compositions with, 634–35 number of, determining, 633-34 Naphthalene, solubility of, 577–78, 578f Newton, 23 Nitrogen liquefaction of, 310f, 311-14 reversible adiabatic compression of, 131–32 Nomenclature, 17 Noncondensable gases. See also Humidification in ideal solution, 480–83 Nonideal solutions, 489–543. See also Activity coefficient excess properties, 489–96 heat effects of mixing, 496–504 molecular view of, 507, 507f problems, 533-43 summary, 531-33 Nonrandom two liquid model (NRTL). See NRTL equation NRTL equation, 520–21 Open systems. See also Balances in open systems defined, 13 ideal and lost work in, 266–71 Operator Δ , 99–100, 255 Osmotic equilibrium, 580-86, 580f desalination and, 585–86 diffusion in, chemical potential and, 582-83 pressure in, 584–85 reverse osmosis, 583-84, 584f Osmotic pressure, 584–85 P° , working with, 608 Partially miscible liquids, 384–89 equilibrium between, 545–48 lever rule and, 388 Pxy graph of, 387f, 552-54, 553f qualitative-phase diagram of, 388-89, 389f Txy graph of, 385f, 554–56, 554f, 557f Partial molar, 405, 408–9 Pascal, 23 Path, 18–19, 18f defined, 18 illustration of, 18f Paths in first law, 101–8 alternate, 106-7, 107f constant-pressure cooling, 104-5 constant-pressure heating, 102-3 constant-temperature process, 107, 108 constant-volume cooling, 102

constant-volume heating, 101-2 enthalpy of steam, 103-5 heat as path function, 105–6 integration, 109–10 in isothermal compression of steam, 108 work as path function, 105–6 Peng-Robinson equation compressibility factor in, 67 fugacity calculated from, 352, 353 fugacity from, 446-47 residual properties from, 232t Perry's Chemical Engineers' Handbook (Perry), 220, 233, 234, 275, 338, 357, 362t Phase behavior of mixtures, 369-400 azeotropes, 380-81 compositions at bubble and dew point, 374f distillation, 378, 379f flash separation, 375-76, 376f flash units, multiple, 377–78 lever rule in, 372-73 partially miscible liquids, 384-89 problems, 394–400 Pxy graph, 373-79 summary, 393 ternary systems, 390-93 Txy graph, 370–73 VLE at elevated pressures and temperatures, 383-84, 384f xy graph, 381–83, 382f Phase change, entropy and, 153-58, 157f constant-pressure path, no phase change, 153 - 54constant-volume path, no phase change, 154 energy balances with, using C_P and $\Delta H_{\rm vap}$, 158 - 59Phase diagrams. See also Pure fluids, phase diagrams of of acetic acid/water/methylisobutyl ketone, 390f from equations of state, 356-58 of ethylene, 356-58 in Raoult's law, 473-74, 474f Phase equilibrium chemical equilibrium and VLE, 625–28 as chemical reaction, 628-29 reactions and, 624–29 Phases, calculating incompressible, 220–21 Phase splitting Gibbs free energy and, 548–56, 550f equilibrium and stability in, 551–52, 551f Phase transitions, 8–9 Pipe, flow through, 272-76 energy losses in, schematic for calculating, 273f pressure drop, 275–76

Pitzer method compressibility factor in, 48, 71 for heat of vaporization, 121-22 in phase diagrams of pure fluids, 47, 48 Planck, Max, 178 Potential energy, 90 Pound-mol (lb-mol), 24 Power, 25t Power generation in open systems, 295–300 Poynting equation, 345–47 PR equation. See Peng-Robinson equation Pressure, 7-8, 22-23, 25t in equilibrium composition, effect of, 623 - 24Henry's law and, 569 irreversible expansion against, 138 Pressure, effect on heat capacities, 113–19, 113f compressed liquid properties, 117–19, 118f constant-pressure cooling of liquid, 115–17 heat capacity of steam, 114-15 ideal-gas heat capacity, 114 liquid heat capacities, 114 Pressure-enthalpy chart, 242-43, 243f Pressure-explicit relations, 228–30 enthalpy, 229 entropy, 229-30 Pressurizing, 321 Processes, 18–19, 18f defined, 18 energy requirements of, calculating, 5 entropy and, 176–77 Properties, 16–17 defined, 16–17 extensive and intensive properties, 16-17 fixed, 17 molar, 16-17 nomenclature and, 17 of pure component, 17 specific, 16-17 tabulated values of, 40-43 Properties, calculating, 205 cubic equations, application to, 230–34 differentials, integration of, 213–14 enthalpy, 217-19 entropy, 217-19 fundamental relationships, 214–17 generalized correlations, 235-36, 237-38f ideal-gas state, 219–20 in compressible phases, 220–21 pressure-explicit relations, 228–30 problems, 246-50 of reference states, 236, 239-42 residual properties, 222–28 summary, 245-46

Properties, calculating (*Continued*) thermodynamic charts, 242–45 thermodynamics, 205–12 Properties of Gases and Liquids, The (Polling, Prausnitz, and O'Connell), 38, 114, 121 PT graph of pure fluid, 36–40, 37f Pure component multicomponent mixture, state of, 18 property of, 17 state of, 17-18 Pure fluid, 337-66 fugacity, 343-53 phase diagrams from equations of state, 356 - 58problems, 360-66 saturation pressure from equations of state, 353 - 56summary, 358-60 two-phase systems, 337–40 VPE of, 340-43 Pure fluids, phase diagrams of, 29–85 compressibility factor, 43-45, 45f corresponding states, 45, 46f empirical equations, 57 PVT behavior of, 29–40 tabulated values of properties, 40-43 virial equation, 53 PV graph of pure fluid, 31–36, 31f critical point, 33 ideal-gas state, 33–34 two-phase region and lever rule, 34–36, 35f PVT behavior boiling in open air, 32 PT graph of pure fluid, 36–40, 37f of pure fluids, phase diagrams of, 29–40 PV graph of pure fluid, 31–36, 31f PVT surface of pure fluid, 30f PVT surface of pure fluid, 30f PV work, 90–96, 91f equation for, obtaining, 90-91 in expansion, 92–93 in isothermal compression of steam, 94–95, 96f reversible, 91–92, 92f Soave-Redlich-Kwong equation used for, 93 - 94Pxy graph, 373–79 of CO_2/n -pentane calculated using Soave-Redlich-Kwong, 451f, 452–53 of completely immiscible liquids, 561–62, 562f of ethanol/water at elevated temperatures, 384f of experimental activity coefficient, 515f

of heptane and decane, 375f forisobutane/furfural system, 389f of partially miscible liquids, 387f, 552-54, 553f reconstructing from limited data, 517, 518 - 19for UNIFAC equation, 530f, 531f UNIQUAC equation used to calculate. 524-25, 526f Quantities relating to entropy, measurable, 151 - 53Quasi-static process, 19-22, 20f example of, 21-22 explained, 21 reversible, 20-21 Rackett equation, 73 Rankine (R), 23 Rankine power plant, 295–300, 295f Raoult's law, 466–74 bubble and dew pressure in, 469–70 bubble T calculation in, 467 deviations from, 508-10, 509f dew P calculation in, 467–68 dew T calculation in, 468 flash calculation in. 468–69 fugacity and, 470-71 hypothetical liquid state in, 472 phase diagram in, 473–74, 474f Reactions, 593–645 activity, 606-13 energy balances in, 601-6 equilibrium composition, 622–24 equilibrium constant, 614–20 equilibrium involving solids, 629–32 multiple, 632-35phase equilibrium and, 624–29 problems, 637-45 standard enthalpy of, 596-601, 599f stoichiometry, 593–96 summary, 636-37 Real mixtures chemical potential in, 440 compression of, 427 properties of, 424–25 Redlich-Kister expansion, 495–96 Reference states calculating, 236, 239-42 using, 240-41 Refrigerants, 307-9 ASHRAE designation of, 307t environment and, 308–9 saturation pressure of, 308f

Index

Refrigeration, 301-9 ammonia refrigerator, 304-6 cycle on PH graph, 303f household refrigerator, 304 refrigerants, 307-9 thermodynamic analysis of, 302-6 vapor-compression refrigeration cycle, 301f Relative humidity (RH), 482, 483 Relative volatility, 382 Residual molar, 408-9 Residual molecular interactions, 507 Residual partial molar, 408–9 Residual properties, 222–28 applications, 225-28 from corresponding states, 235–36 from cubic equations of state, 232-34, 232t defined, 22 enthalpy, 223 entropy, 224 in ideal-gas state, 225-26 of methane, using virial coefficient, 227–28 of mixtures, 420, 421 other, 224-25 from truncated virial equation, 226-27 volume, 224 Reverse osmosis, 583-84, 584f Reversible PV work, 91-92, 92f Reversibility, entropy and, 176–77 Reversible adiabatic processes, 127–30, 131-32, 132f in entropy balance, 260–61 in ideal-gas state, 164-66 in mixing, 134-36 in nitrogen compression, 131–32 in steam compression, 165 Reversible quasi-static process, 20–21 Roots in compressibility factor, acceptable, 63, 66, 67 of cubic equation of state, 63-65 Saturated liquid, fugacity of, 346 Saturation pressure from equations of state, 353-56, 354f, 355f Second law alternative statements of, 177-82 Carnot cycle analyzed by, 171 in closed system, 150–53 consequences of, 180, 200-201 defined, 149 direction of heat flow determined by, 184-85 entropy and, 149-204 in feasibility of process, 185-87 Sensible heat, 109

Separation of work, ideal solution in, 464 Separation units, 4f, 5 Shaft work, 90, 91f Sign convention for heat, 97 for transfer energy, direction of, 89 for work, 89 Simple interpolations, 41, 41f Simple system, 13 SI system of units, 22 energy measured in, 24 mole, 24 pressure measured in, 22–23 temperature measured in, 23 Soave-Redlich-Kwong equation binary mixture properties using, 423t binary VLE using, 452–53 calculation of Henry's law constant, 569–70, 571f CO_2/n -pentane calculated using, 451f, 452 - 53coefficient of thermal expansion using, 207-9 compressibility factor in, 61 fugacity from, 352, 353, 446-48 heat of vaporization using, 338 for PV work, 93–94 residual properties from, 232-34, 232t vapor-liquid mixture calculated by, 339-40 Solids activity of, 609-10, 612 entropy of, 155-56, 157 in liquids, solubility of, 575-80 Solubility of benzene, 577-78, 578f eutectic point, 579-80 of gases in liquids, 563-74 limits using activity coefficients, 547-48 of naphthalene, 577-78, 578f of solids in liquids, 575-80 Solute, activity of, 609, 611–12 Specific energy, 25t Specific heat, 111 Specific property, 16–17 SRK equation. See Soave-Redlich-Kwong equation Stability, 355-56 entropy and, 191–95 equilibrium and, in phase splitting, 551–52, 551f mathematical conditions for, 552 Standard state, activity and, 610, 613 State function, 17 constant-volume heat capacity as, 109, 113 enthalpy as, 103, 125–26 entropy as, 153

State function (*Continued*) heat capacity as, 109 internal energy as, 89, 96, 107 Statistical thermodynamics, 11–13 Steady state energy balance, 258 entropy balance, 260, 261 vs. equilibrium, 261 Steam in Carnot cycle, 175-76 Carnot cycle using, 175–76 compression of, 291–92 entropy of, 163 filling a tank with, 317–18 fugacity of, 349 tables, 663-75 tables, fugacity from, 347 venting, 322 Steam turbine, 282-87 actual operation, 283 ideal and lost work in, 286-87 Mollier graph used in, 285–86, 285f reversible operation, 283 steam tables used in, 283–84 Stoichiometry, 593–96 Storable energy, 89 Subscripts, 411 Successive interpolations, 42 Summary, 26 Surroundings, in system, 13 System, 13–14 adiabatic, 13 classifying, 13-14 closed, 13 composite, 13 diathermal, 13 equilibriumin, 15–16 examples of, 14f isolated. 13 open, 13 simple, 13 surroundings in, 13 universe in, 13 Tabulated properties entropy calculated using, 162 fugacity calculated using, 347–48 interpolations, 40–43, 41f Temperature adiabatic flame, 605-6 defined, 8 entropy and, 153 in heat transfer, 20f Henry's law and, 569

liquid miscibility and, 556-58 measuring, 23-24 in molecular collision, 7-8 upper consolute, 557 Temperature, effect on heat capacities, 113-19, 113f compressed liquid properties, 117-19, 118f constant-pressure cooling of liquid, 115–17 heat capacity of steam, 114-15 ideal-gas heat capacity, 114 liquid heat capacities, 114 Temperature-enthalpy chart, 243-44, 244f Ternary systems, 390–93 Thermal equilibrium, 15 Thermal expansion coefficient using Soave-Redlich-Kwong, 207-9 Thermodynamic analysis of processes, 314–15 of refrigeration, 302–6 Thermodynamic charts, 242–45 enthalpy-entropy (Mollier chart), 244–45, 245fpressure-enthalpy, 242-43, 243f temperature-enthalpy, 243-44, 244f Thermodynamic cycle, notion of, 169 Thermodynamic potential function, 195 Thermodynamic potentials, 194–95, 195f Thermodynamics chemical, 3–5, 4f definitions, 13-17 development of, 12–13 how and why in, 12-13introduction, 3-5 molecular basis of, 5-11 multicomponent mixture, state of, 18 problems, 26–28 process and path, 18-19, 18f pure component, state of, 17-18 quasi-static process, 19-22, 20f statistical vs. classical, 11–13 summary, 26 units, 22-25 Thermodynamics, calculus of, 205-12 differential and integral forms of a function, 209 - 12thermal expansion coefficient using Soave-Redlich-Kwong, 207-9 triple-product rule in ideal-gas state, 207 Thermodynamics of steady-state processes, 272 - 94adiabatic mixing, 276-78, 277f expansion and compression of liquids, 292 - 94flow through pipe, 272–76 gas compression, 290–92

Index

heat exchanger, 278-81, 279f power generation, 295-300 steam turbine, 282-87 throttling, 287-90 Thomson, William, 100, 178 Throttling, 287–90 of compressed liquid, 288-89, 290f of ideal gas, 288 Time, 25t Torr. 23 Triple-product rule in ideal-gas state, 207 Truncated virial equation, residual properties from, 226–27 Turbines, gas/steam, 282–87 Two-phase systems, pure fluid in, 337–40 condensing a vapor-liquid mixture, 340 heat of vaporization using Soave-Redlich-Kwong, 338 vapor-liquid mixture calculated by Soave-Redlich-Kwong, 339-40 Txy graph, 370-73, 379f of completely immiscible liquids, 559-61, 559f of ethanol/water at elevated temperatures, 384f of heptane and decane, 370f of partially miscible liquids, 385f, 554-56, 554f, 557f UNIFAC equation, 525–31 detailed calculation using, 528–30 Pxy graph for, 530f, 531f terms calculated by, 527–28 using, 530, 532 UNIQUAC equation, 522–25 group contribution method in, 523-24 Pxy graph calculated from, 524–25, 526f Units, 22–25 constants, 22t conversions, 25t energy, 24–25, 25t mole, 24pressure, 22-23, 25t temperature, 23–24 Universal Functional Activity Coefficient (UNIFAC). See UNIFAC equation Universe entropy of, 168 in system, 13 Unsteady-state balances, 315–23 filling a tank with ideal gas, 318–18 filling a tank with steam, 317–18 pressurizing a tank, 315–19, 315f venting a tank, 319–23

venting ideal gas, 322-23 venting steam, 322 Upper consolute temperature (UCT), 557 Vacuum, irreversible expansion against, 136 - 37Van der Waals equation compressibility factor in, 58-60 residual properties from, 232t Van der Waals forces, 6 Van Laar equation, 519 Vaporization. See also Vapor-liquid mixture enthalpy of, 478-79 entropy of, 157, 158 heat of, using Soave-Redlich-Kwong, 338 Vapor-liquid equilibrium (VLE), 369. See also Henry's law; Vapor-liquid equilibrium (VLE) Antoine equation, 343 binary, using Soave-Redlich-Kwong, 452-53 chemical equilibrium and, 625–28 chemical potential, 341 Clausius-Clapeyron equation, 341–43 elevated pressures and temperatures, 383-84, 384f at elevated pressures and temperatures, 383-84, 384f equations in, solving, 449-50, 451f in ideal solution, 466–74 (See also Raoult's law) problems in, classification of, 448-49 of pure fluid, 340–43 Vapor-liquid equilibrium, theory of, 435–59 chemical potential in, 439-42 fugacity in, 443-48 Gibbs free energy in, 435–39 using equations of state, 448–53 Vapor-liquid-liquid equilibrium (VLLE), 546f Vapor-liquid mixture condensing, 340 Soave-Redlich-Kwong equation used to calculate, 339-40 Vapor-liquid separator, 4f, 5 Variables change of, in fundamental relationships, 217 derivatives and integrals with functions of multiple, 110 Venting, 321 ideal gas, 322-23 steam, 322 a tank, 319-23 Virial equation Benedict-Webb-Rubin equation and, 68 calculated isotherms using, 57f

Virial equation (Continued) compressibility factor in, 53, 54, 56 molar volume calculated with, example of, 55–56 residual properties of methane using, 227–28 second virial coefficient, 53–54, 55 summary, 78 truncated, 54, 226–27
Volume, 25t excess properties in, 494–95, 495f residual, 224
Volume of mixing, 409–10
Von Guericke, Otto, 27–28
Wilson equation, 519–20

Work, 88–89, 88f adiabatic production of, 261, 262 heat and, shared characteristics with, 97 ideal, 183–88 lost, in entropy, 183–88, 191 maximum, in feasibility design, 186–87 as path function, 105–6 PV, 90–96, 91f separation of, ideal solution in, 464 shaft, 90, 91f sign convention for, 89 value of heat, Carnot cycle and, 182–83, 182f x, y, z, convention for, 372 xy graph, 381–83, 382f

ZP graph of pure fluids, 43–45, 45f, 56